

TOWN OF WESTFORD  
**PERMANENT TOWN  
BUILDING COMMITTEE**  
TOWN HALL  
WESTFORD, MASSACHUSETTS 01886  
(978) 692-5501

**REQUEST FOR QUALIFICATIONS**

**WESTFORD ACADEMY ATHLETIC COMPLEX  
MASTER PLAN**

**ADDENDUM NO.1**

A Briefing Session was held on Wednesday, September 9<sup>th</sup>, 2015 at 10:00 a.m. at the Westford Academy Athletic Complex. A tour of the facilities was provided to all attendees. The following documents are being provided to all registered firms:

1. Briefing Session Attendance Sheet (see attached)
2. Zone II Delineation Report – prepared by Dufresne-Henry, Inc., May 2006.
3. Wastewater Treatment Facility Plans

The Zone II Report and Treatment Facility Plans are available to be downloaded directly off the Town of Westford website.

[http://www.westfordma.gov/Pages/Government/WestfordMA\\_Procurement/list](http://www.westfordma.gov/Pages/Government/WestfordMA_Procurement/list)

All documents are being provided for information purposes only.

**All proposals must be received at the Westford Public Schools Office, 23 Depot Street, Westford, MA 01886 by no later than 2:00 p.m. on Friday, September 18, 2015.**

All proposals must be submitted in a sealed envelope, clearly marked as follows:

**REQUEST FOR QUALIFICATIONS**  
**WESTFORD ACADEMY ATHLETIC COMPLEX**  
**MASTER PLAN**

Everett V. Olsen, Jr.  
Superintendent of Schools  
Westford Public Schools  
23 Depot Street  
Westford, MA 01886

**End of Addendum No.1**

ATTENDANCE SHEET

**Westford Academy Athletic Complex Master Plan – Request for Proposals**

**Briefing Session**

**Location:** Westford Academy, 60 Patten Road, Westford, MA

**Date:** Wednesday, September 9<sup>th</sup>, 2015 - 9:00 a.m.

Name	Representing	Email
1. Thomas J. Mahanna	Permanent Town Building Committee	<a href="mailto:tmahanna@westfordma.gov">tmahanna@westfordma.gov</a>
2. Dan Twomey	Westford Academy Athletic Dept.	<a href="mailto:dtwomey@westfordk12.us">dtwomey@westfordk12.us</a>
3. James Antonelli	Westford Academy	<a href="mailto:jantonelli@westfordk12.us">jantonelli@westfordk12.us</a>
4. Kathy Auth	Westford School Department	<a href="mailto:kauth@westfordk12.us">kauth@westfordk12.us</a>
5. Stephen Cronin	Westford Water Department	<a href="mailto:scronin@westfordma.gov">scronin@westfordma.gov</a>
6. Danielle Spicer	Green International Affiliates	dspicer@greenintl.com
7. Rachel Amato	JJA Sports	rAmato@jjasports.com
8. Bob Sykes	PARE CORPORATION	bsykes@parecorp.com
9. Bill Seymour	GALE	wjs@gainc.com
10. J. MICHAEL SULLIVAN	BEACON ABCA. ASSOC.	jms@beaconarch.com
11.		

## **SECTION THREE ZONE II DELINEATION**

### **3.1 INTRODUCTION**

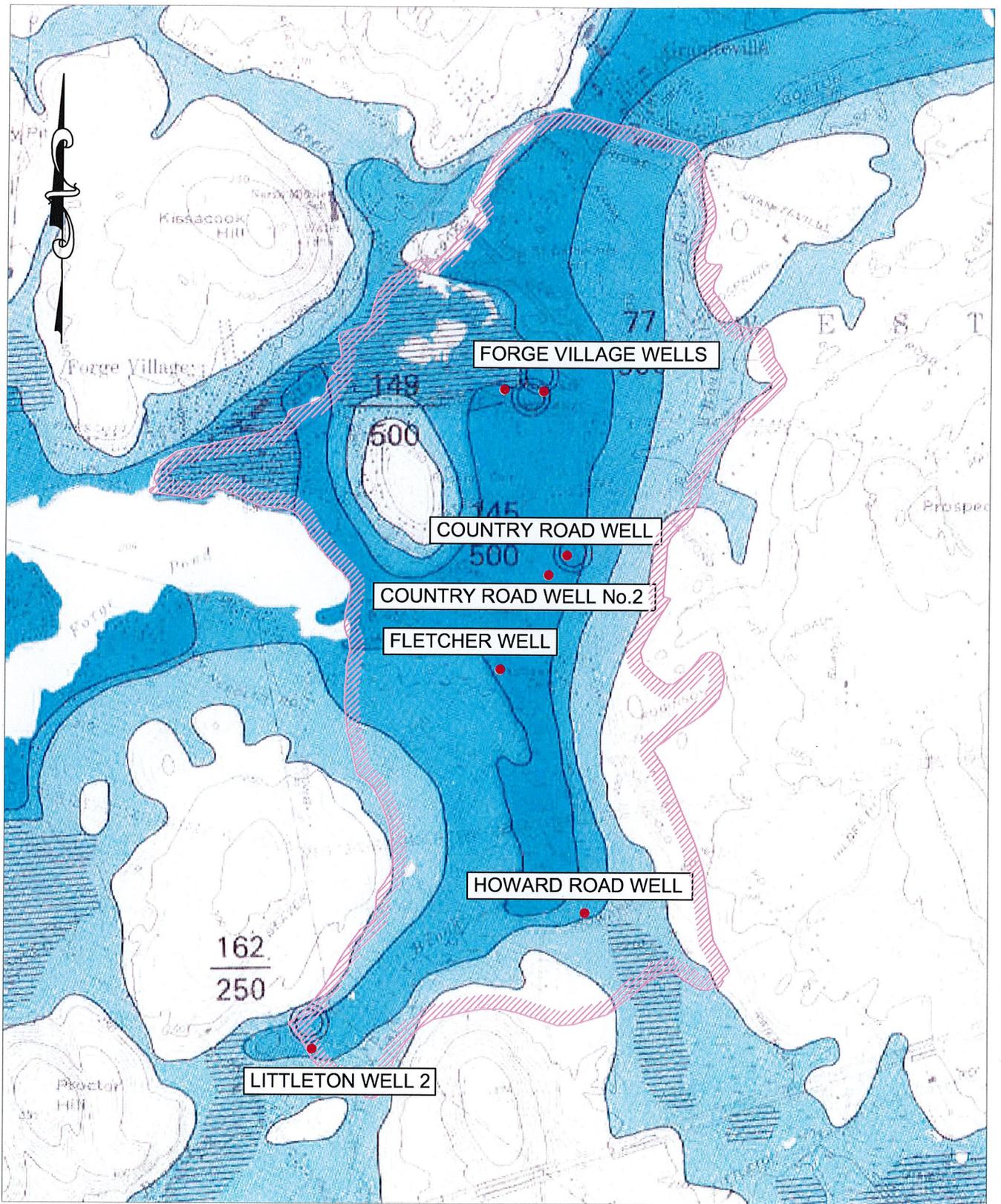
To delineate the Zone II for the proposed Country Road Well No.2, a computer model was developed using the U.S. Geological Survey Modular Finite-Difference Groundwater Flow Model (MODFLOW). This model was used to determine the area of the regional aquifer that contributes water to the proposed well under severe pumping and recharge conditions.

### **3.2 CONCEPTUAL MODEL**

The Beaver Brook Aquifer is a valley-fill aquifer created by the deposition of sand and gravel from glacial meltwater flowing in a pre-existing valley in the bedrock. These permeable stratified-drift deposits extend from Littleton through Westford and Chelmsford to the Merrimack River. These deposits are bounded by upland areas mantled by glacial till. Till has much lower hydraulic conductivity than the outwash deposits and is not considered an aquifer deposit. The USGS mapped limit of the aquifer is shown in Figure 3-1.

The glacial outwash aquifer is fed by local recharge and by recharge and runoff from the neighboring hillsides. Stony Brook and other surface water courses are generally gaining streams into which groundwater discharges. Thus near the wells, in the absence of pumping, groundwater flows from the surrounding hills into Stony Brook and its tributaries. The aquifer is bounded by local surface water divides for the surface water basin draining to Stony Brook and its tributaries. In the absence of pumping withdrawals, the groundwater divide would tend to mirror the overlying surface water divide.

Well logs for pumping and observation wells installed in the vicinity of the Country Road Well No.2 site indicate the presence of stratified sand and gravel, and fine sand and silt. Outwash deposits extend to at least 90 feet deep in the aquifer, but are generally in the range of 30 to 60 feet thick.



FROM USGS HA-662

 EXISTING ZONE II  
DELINEATION

**FIGURE 3-1**



**Dufresne-Henry**  
Westford, Massachusetts  
Tel. (978) 692-1913  
www.dufresne-henry.com

WESTFORD WATER DEPARTMENT

**BEAVER BROOK AQUIFER  
PROPOSED COUNTRY ROAD No.2**

Project No.	9105031
Proj. Mgr.	DGH
Scale	1"=2000'
Date	MAY 2006

WESTFORD

MASSACHUSETTS

A

11:34:31 aquifer, wood, VI S01MA ser7750  
 11:34:31 aquifer, wood, VI S01MA ser7750  
 11:34:31 aquifer, wood, VI S01MA ser7750  
 11:34:31 aquifer, wood, VI S01MA ser7750

An areal or two-dimensional model of the glacial drift aquifer is appropriate for determining the groundwater flow in the project area because the aquifer is a single layer of outwash deposits and vertical flows are not relevant for identifying the zone of contribution.

### 3.3 GROUNDWATER MODEL DESCRIPTION

The groundwater flow model of the Beaver Brook Aquifer was developed using the U.S. Geological Survey (USGS) MODFLOW computer program. The model determines the distribution of hydraulic head and the ground-water flow field over time and space. The model considers:

- the varying capacities of the geologic materials to transmit groundwater flow, represented by the aquifer transmissivity;
- the changes in the quantity of water stored in the geologic materials, represented by the aquifer storage coefficient; and
- the influence of boundary conditions where water enters or leaves the groundwater system.

Typical boundary conditions are wells, streams, springs, and impermeable barriers to flow. The water table is also a boundary through which rainfall or other recharge enters the groundwater system.

MODFLOW is described by its authors as a modular computer program for three-dimensional groundwater flow modeling (McDonald and Harbaugh, 1988). "Modular" refers to the structuring of the computer programming code into independent sub-programs or modules, each performing a distinct, well-defined task. One or more modules together form the major code capabilities, or "packages." Individual packages address specific aspects of the groundwater system. The MODFLOW packages used for this model are as follows:

Basic package - establishes basic model structure and computer code bookkeeping and output instructions. The basic package is required for use in all MODFLOW applications.

Block-centered flow package - establishes the geometry and hydraulic properties of the model grid. The block-centered flow package is required for use in all MODFLOW applications.

River Package - represents a river underlain by a variable permeability bottom. A riverbed conductance parameter must be specified in using a river package.

Recharge package - specifies the rate of rainfall recharge into the surface of the modeled area.

Well package - represents withdrawal wells (negative flow in model input), recharge wells (positive flow), and specified-flow boundary conditions.

Strongly implicit procedure (SIP) package - one of several available packages with which to solve the groundwater flow equations. The SIP is an accelerated solution technique that solves most problems more quickly than the other packages.

The MODFLOW code provides several computation options. In representing processes over time, the model can be operated as a steady-state (not varying in time) or transient (varying in time) model. In this study, the model was run in steady-state mode to evaluate long-term average behavior of the groundwater system. MODFLOW permits the vertical geometry to be represented as fully three-dimensional, quasi-three-dimensional, or two-dimensional. In the quasi-three-dimensional option, aquifers are represented as model layers, but separating confining units are modeled through interlayer leakage coefficients rather than as explicit model layers. In the fully three-dimensional option both aquifer units and confining units are explicitly represented in the model layer structure. In the two-dimensional model a single model layer is specified. A two-dimensional formulation is used in this study.

### **3.4 MODEL DEVELOPMENT**

The development of a groundwater flow model entails preparing the geological information from the conceptual model in a form usable by the MODFLOW computer program. This preparation included the following:

- subdividing the model horizontal area into a grid of computation elements;
- specifying boundary conditions in the model domain; and
- assigning values of physical properties such as transmissivity to the resulting two-dimensional array of model cells.

The input data required by the model include

- geographical definition of the model area and model computation grid;
- model boundary conditions (no-flow, specified-flow, river, and constant head boundaries);
- distribution of the hydraulic parameters, the aquifer transmissivity, and storage coefficient;
- location and pumping rate of wells; and
- amount of precipitation recharge.

Model Area and Boundaries - The model area is shown in Figure 3-2. Most of the model boundaries are placed at the natural boundaries of the aquifer where the sand and gravel deposits meet the glacial till as mapped by the USGS in HA-662 (Brackley and Hansen, 1985). Other no-flow boundaries are located at the drainage basin boundary, surface water bodies, or far enough from the pumping wells to ensure no effect on the zone of influence.

Internal boundaries are typically surface-water features that interact with the ground-water system. Beaver Brook is represented in the model using the MODFLOW river package. Stream elevations were determined using the U.S. Geological Survey topographic maps. Stream elevations were specified at points where contours on the topographic map cross the stream. Elevations in the model were linearly interpolated between the map points.

The MODFLOW river package considers the stream to be underlain by a stream bed of variable conductance. The stream conductance,  $C$ , for each river cell was calculated using the following equation:

$$C = K L W / M$$

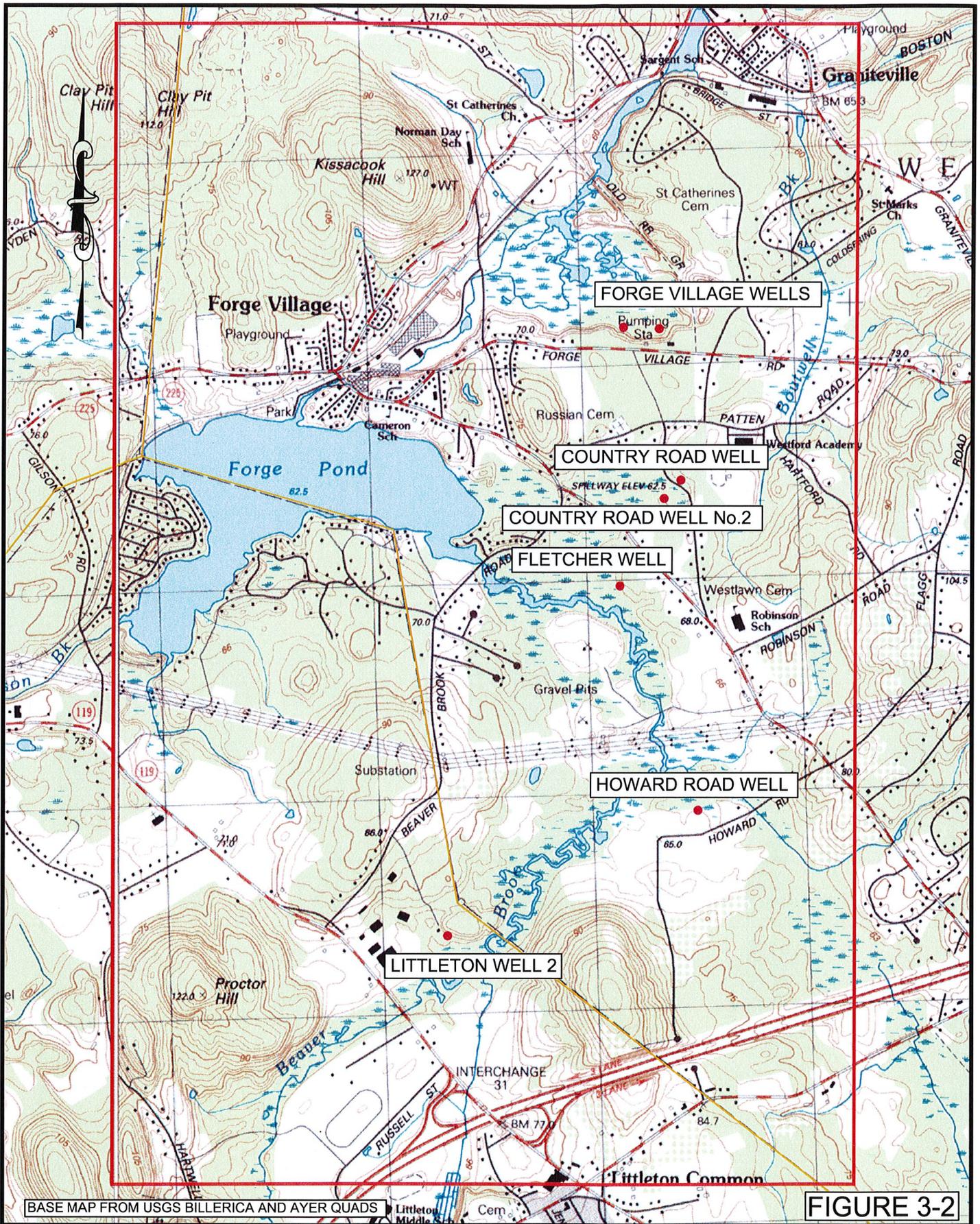
Where:

$K$  = hydraulic conductivity of the stream bed material

$L$  = length of stream within the cell

$W$  = width of stream, and

$M$  = thickness of the stream bed material.



BASE MAP FROM USGS BILLERICA AND AYER QUADS

**FIGURE 3-2**



WESTFORD WATER DEPARTMENT

**MODEL AREA  
PROPOSED COUNTRY ROAD No.2**

WESTFORD MASSACHUSETTS

Project No.	9105031
Proj. Mgr.	DGH
Scale	1"=2000'
Date	MAY 2006
A	

1 (WES) : of Site : dhanwc : 2006 1' : 2 model : VST-FSC : P-Phase

For the ponds and the streams, the stream bed hydraulic conductivity was assumed to be 2.0 feet/day, a value consistent with those reported by de Lima (1991) for small sandy bottom streams in New England.

The existing Westford Water Department wells in the model area are also represented as a boundary in the model with the well package. The Town of Littleton Well 2 is located in the model area and was included in the simulations. The wells in the model were set to the 2005 average rates in order to simulate the overall average baseline groundwater flow in the aquifer. The results from the average conditions simulation were used as the starting conditions for the transient Zone II simulation with the wells pumping their maximum approved yield. Pumping rates used in the model are given in Table 3-1.

**Table 3-1  
Pumping Rates Used in Model  
(Million Gallons per Day)**

Well Name	Starting Conditions (Average Rate*)	Zone II Simulation (Max Rate)
Forge Village 1	0.135	0.34
Forge Village 2	0.280	0.59
Country Road	0	0**
Country Road 2	0	0.61
Fletcher	0.316	0.69
Howard Road	0.191	0.43
Littleton Well 2	0.200	0.41

\* Based on 2005 DEP report. Estimated for Littleton Well 2.

\*\* The approved Zone II rate for the Country Road Well is 0.54 MGD.

No private wells are believed to exist near the project site. Private wells are almost exclusively deep bedrock wells with relatively small yields. Furthermore, any groundwater extracted from them would be almost entirely discharged on site through private septic systems resulting in essentially no impact to the groundwater system. For these reasons, no private wells were modeled.

The numerical model grid used by the computer program must be a rectangular area, therefore there are inactive grid cells between these boundaries and the limits of the numerical grid. The limit of the active grid cells and boundary conditions are shown in Figure 3-3. A detail of the well area with the calibration targets is given in Figure 3-3A.

Hydraulic Parameters - The distribution of aquifer transmissivity in the model is shown in Figure 3-4. This distribution is directly from the U.S. Geological Survey Hydrologic Atlas HA-662. The transmissivity values used in the model are based on the results of the pumping test and model calibration and are in the ranges indicated by HA-662. A storage coefficient of 0.09 was assigned to the entire model area based on model calibration and aquifer test data. This value is consistent with unconfined conditions.

Recharge - The recharge rate used for precipitation in the model was 21-inches per year which is one half the average annual precipitation for this area. One half the precipitation is accepted as the amount to recharge sandy aquifers in New England after losses of runoff and evapo-transpiration.

### **3.5 MODEL CALIBRATION**

The model was calibrated to results from the pumping test. The observed drawdown in six observation wells during the test at 425 GPM was compared to results from a simulation of the test. Minor adjustments to transmissivity and storativity values in the model were made until the residual mean of observed and calculated drawdowns could not be further improved. Observed and simulated drawdown for each observation well in the pumping test is shown on Chart 3-1. Most calculated drawdown curves match observations favorably. Observed vs simulated drawdown is shown on Chart 3-2. The overall residual mean of observed and calculated drawdowns is 0.20 feet indicating good model calibration.

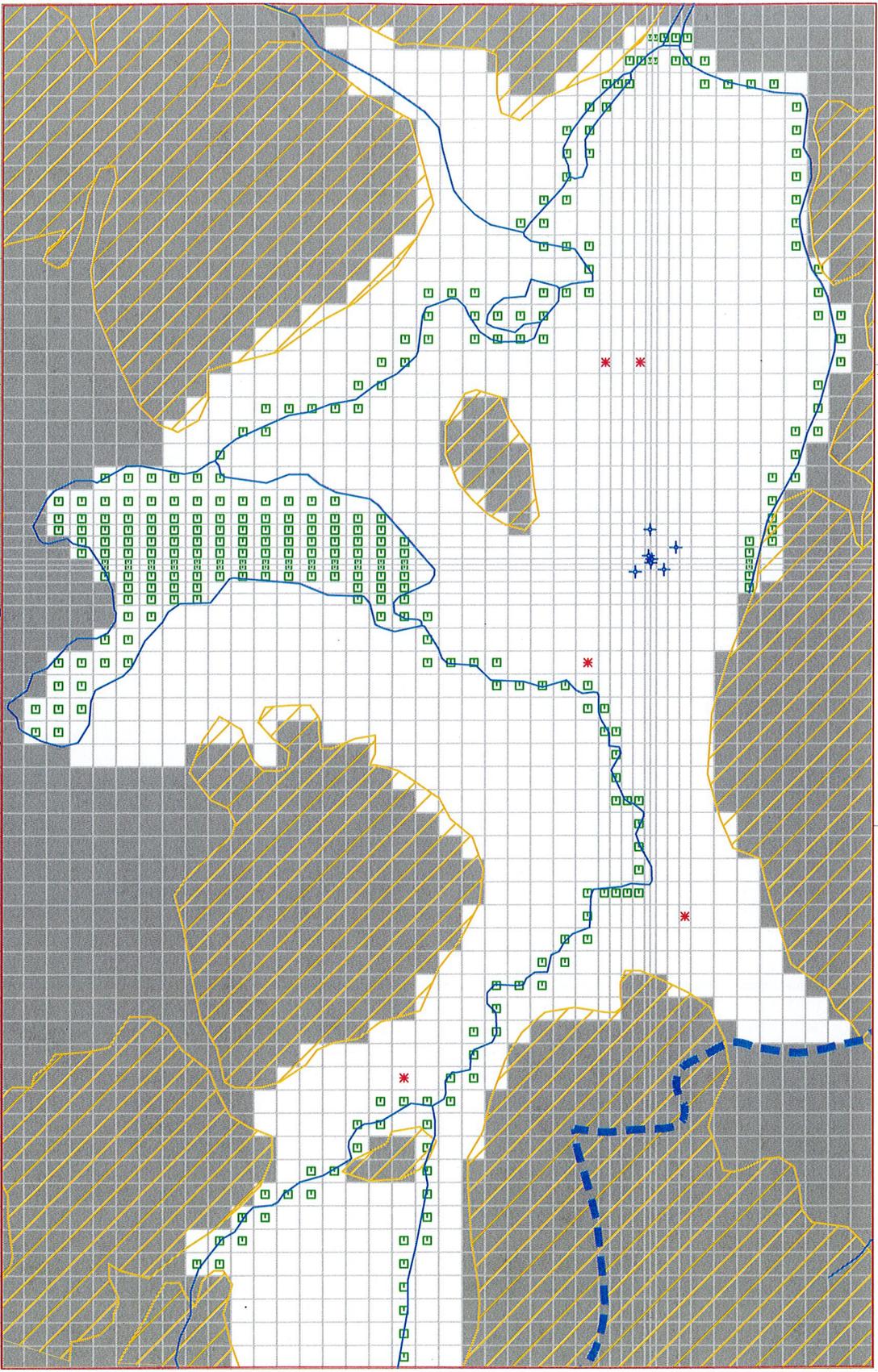


PHYSICAL FEATURES

BASIN BOUNDARY

RIVER

GLACIAL TILL



BOUNDARY CONDITIONS

\* WELL

□ RIVER

■ NO FLOW

+ CALIBRATION TARGET

MAPPING FROM USGS HA-662 AND MASS GIS

**FIGURE 3-3**

**Dufresne-Henry**  
Westford, Massachusetts  
Tel. (978) 692-1913  
www.dufresne-henry.com

WESTFORD WATER DEPARTMENT

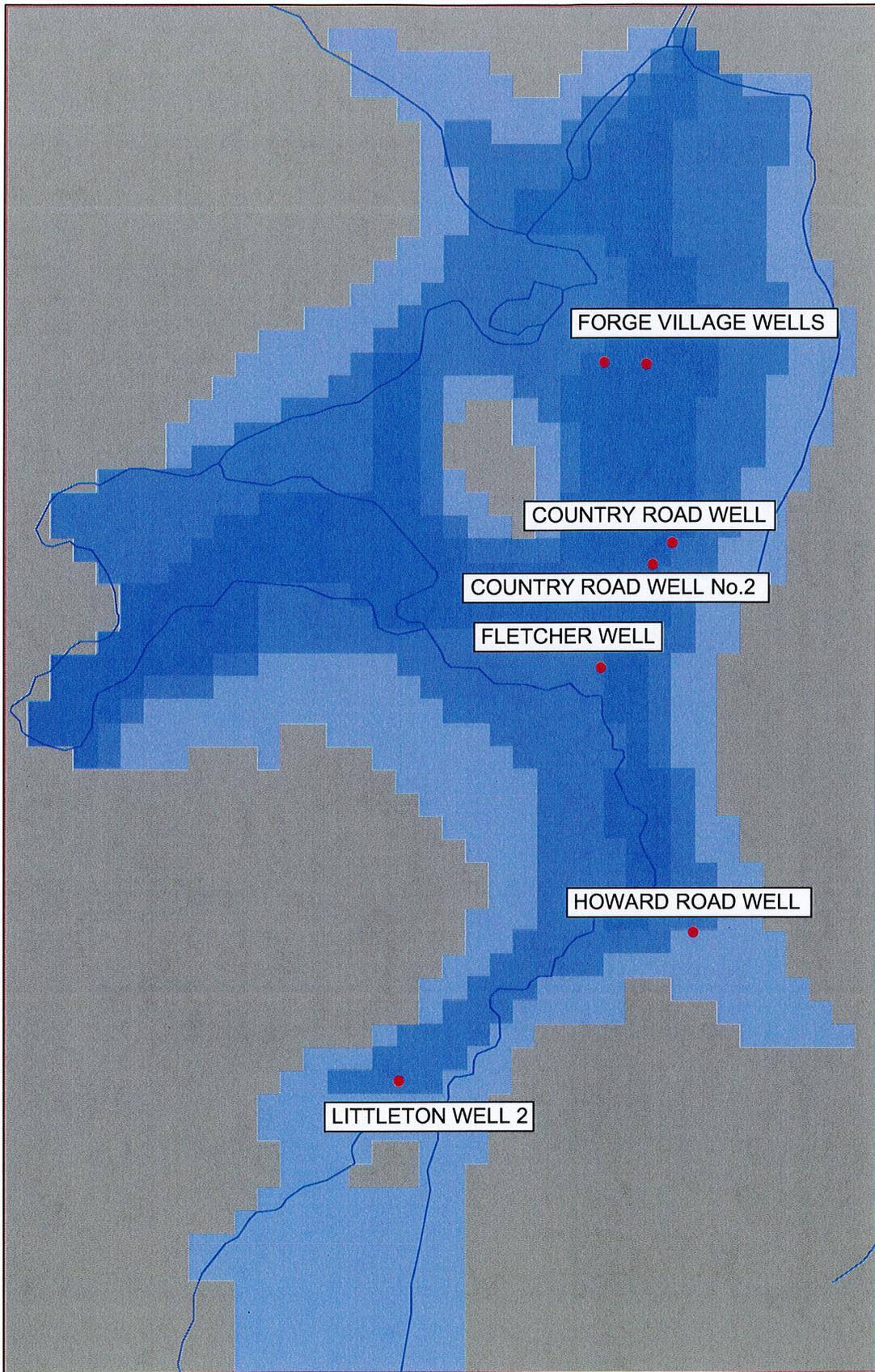
**MODEL GRID AND BOUNDARY CONDITIONS  
PROPOSED COUNTRY ROAD No.2**

WESTFORD MASSACHUSETTS

Project No.	9105031
Proj. Mgr.	DGH
Scale	1"=2000'
Date	MAY 2006
A	

31 (WE) M.D. - D  
Civil/fig. 3-3 grid. 11:35:33 wood, 1/11 S011MA-er7750





750 SQ FT/DAY



3500 SQ FT/DAY



7500 SQ FT/DAY

BASED ON USGS HA-662

**FIGURE 3-4**



Westford, Massachusetts  
Tel. (978) 692-1913  
www.dufresne-henry.com

WESTFORD WATER DEPARTMENT

**TRANSMISSIVITY DISTRIBUTION  
PROPOSED COUNTRY ROAD No.2**

WESTFORD

MASSACHUSETTS

Project No.	9105031
Proj. Mgr.	DGH
Scale	1"=2000'
Date	MAY 2006

A

\\www31\WES\...M.D. - Development of Site - \www31\fig\...eng, and trans...at...2006 11\...dhanwood, ...ST-FS01...-Phase7...

CHART 3-1

MODEL CALIBRATION

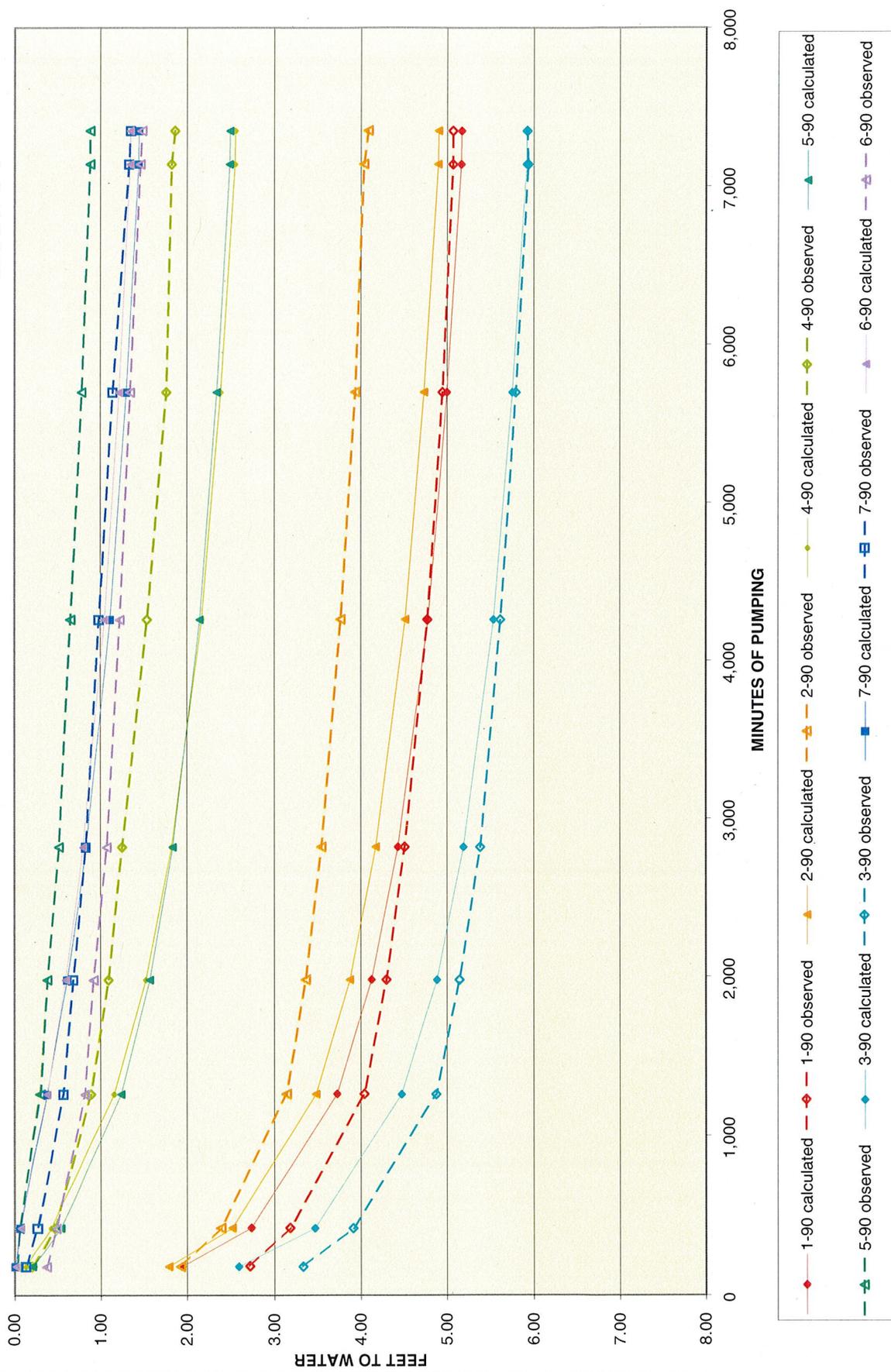
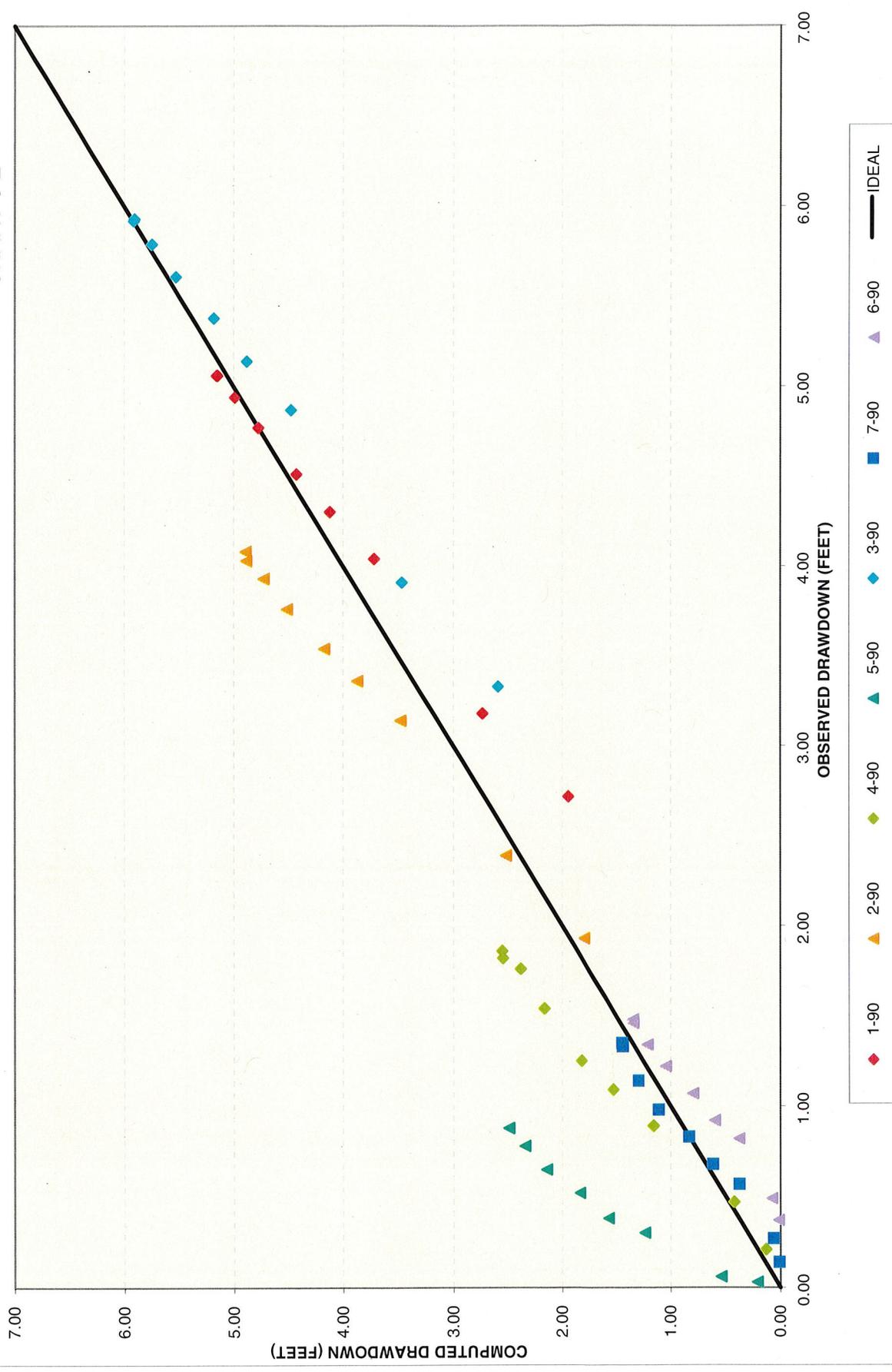


CHART 3-2

MODEL CALIBRATION

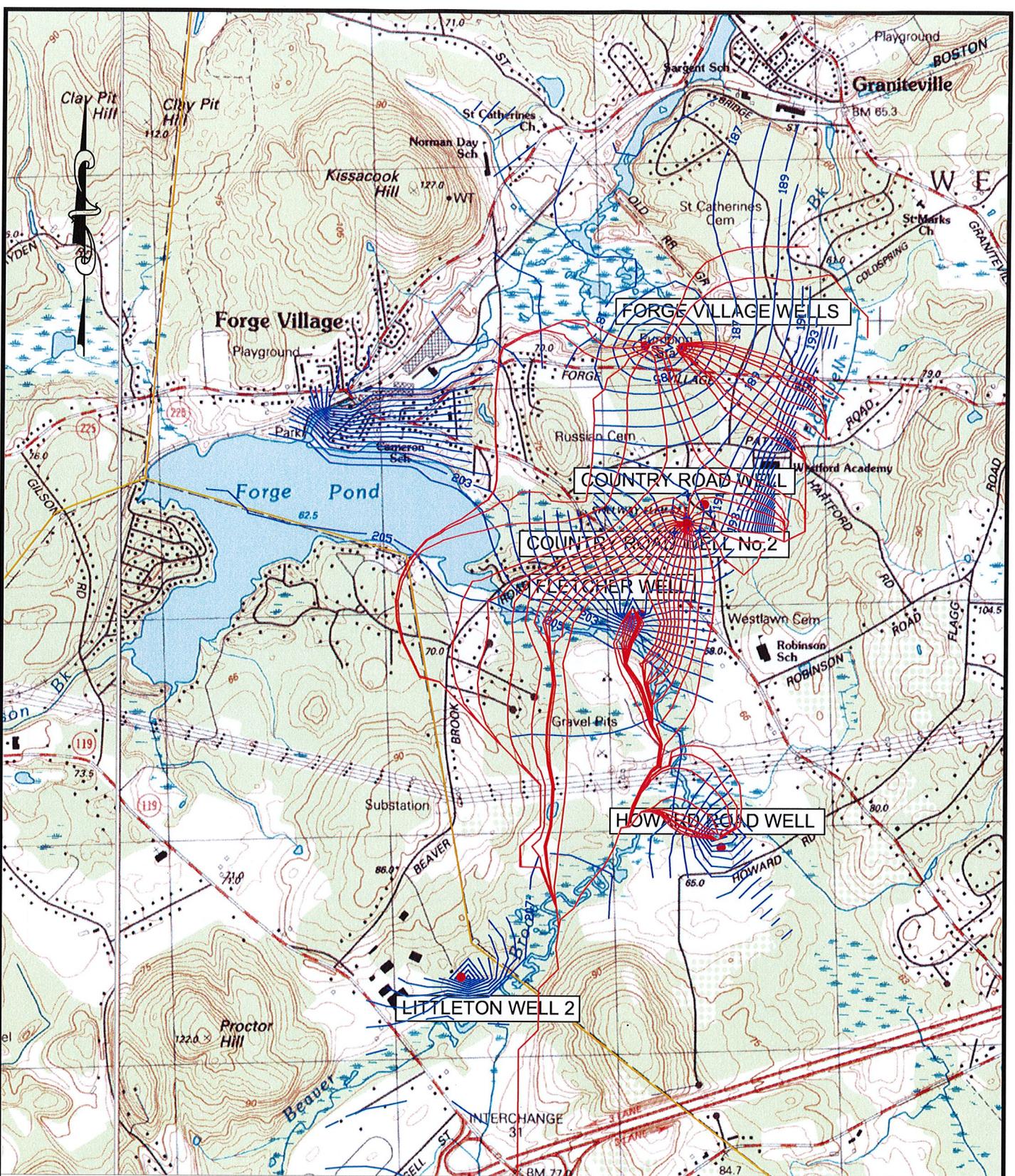


### **3.6 MODEL RESULTS**

To delineate the Zone II, the model was used in transient mode to simulate groundwater flow for 180 days of pumping with no recharge. Starting conditions for the Zone II simulation were constructed in a steady-state model simulation with 21-inches per year of recharge and the existing wells pumping at average rates. The Zone II simulation used maximum approved pumping rates and no recharge. The U.S. Geological Survey MODPATH particle-tracking model was applied to the potentiometric surface predicted by MODFLOW to backtrack groundwater flow to the source of the water reaching the well. A total of 10 particles were tracked distributed around the pumping well at a radius of 50 feet.

Contours of hydraulic head and particle tracks predicted by the model are provided in Figure 3-5. The Zone II is delineated in Figure 3-6 as a composite of the results shown in Figure 3-5 and the existing Zone II (Figure 3-1). The portions of the model results Zone II that did not encompass the existing Zone II were included to prevent the Zone II boundary from becoming smaller.

All original MODFLOW input and output files are included on disk in Appendix E.



BASE MAP FROM USGS BILLERICA AND AYER QUADS

**FIGURE 3-5**

WESTFORD WATER DEPARTMENT

**MODEL RESULTS  
PROPOSED COUNTRY ROAD No.2**

Project No.	9105031
Proj. Mgr.	DGH
Scale	1"=2000'
Date	MAY 2006
A	

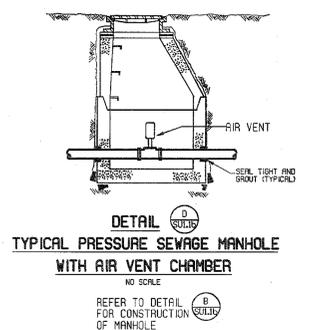
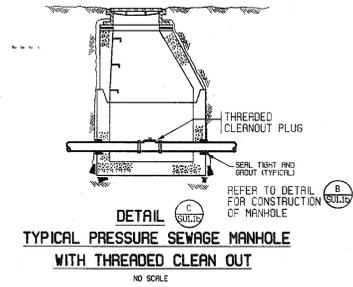
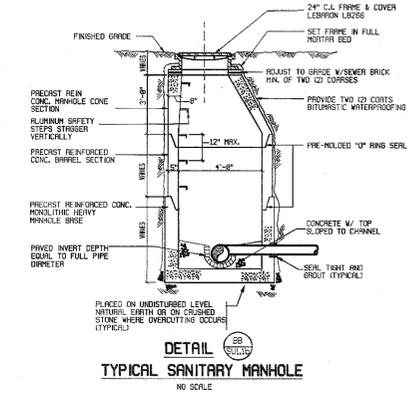
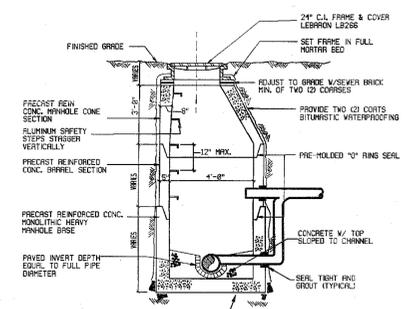
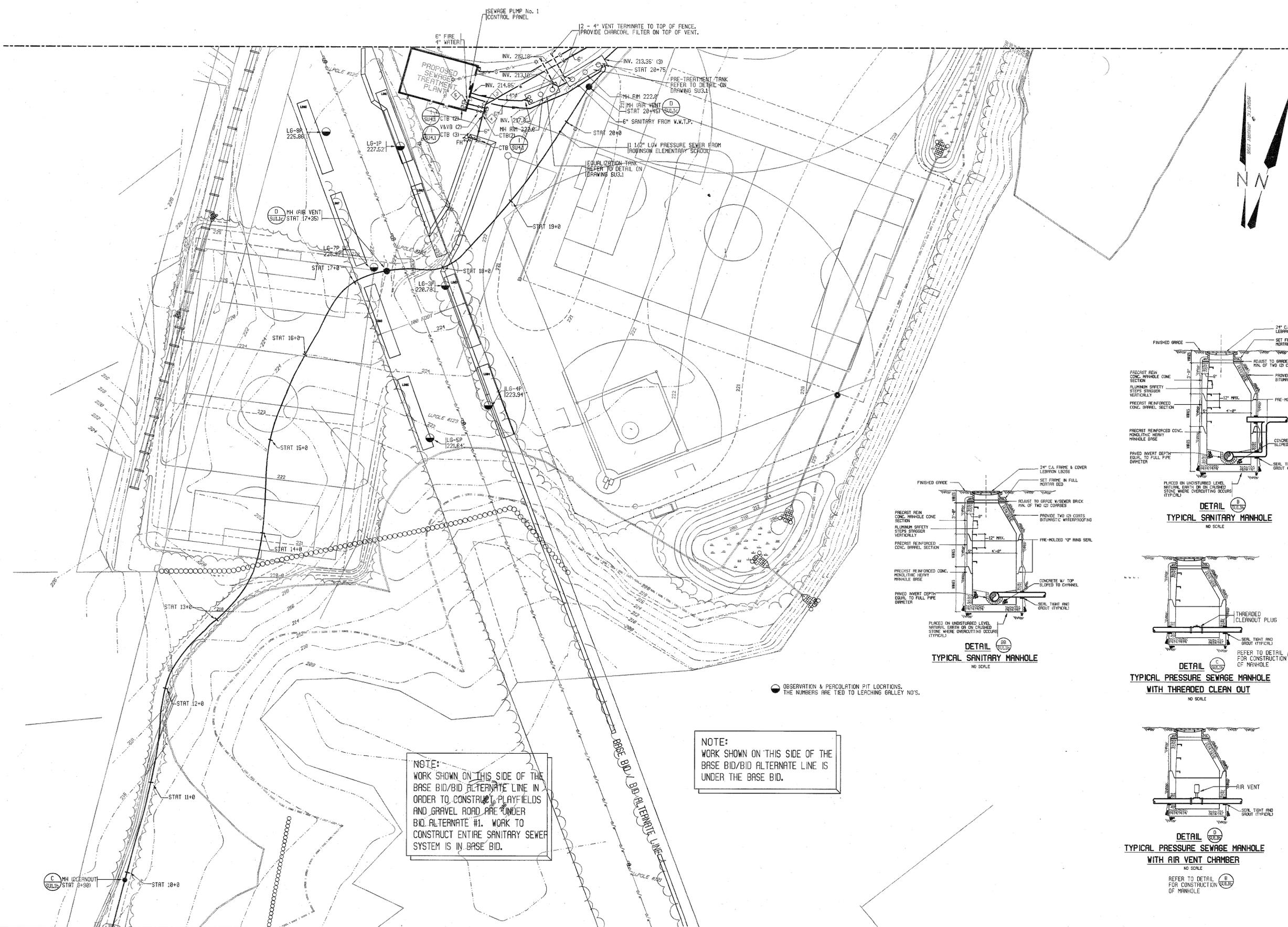


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WESTFORD

MASSACHUSETTS





**NOTE:**  
WORK SHOWN ON THIS SIDE OF THE  
BASE BID/BID ALTERNATE LINE IN  
ORDER TO CONSTRUCT PLAYFIELDS  
AND GRAVEL ROAD ARE UNDER  
BID ALTERNATE #1. WORK TO  
CONSTRUCT ENTIRE SANITARY SEWER  
SYSTEM IS IN BASE BID.

**NOTE:**  
WORK SHOWN ON THIS SIDE OF THE  
BASE BID/BID ALTERNATE LINE IS  
UNDER THE BASE BID.

**BASE BID NOTES**

- ALL SANITARY WORK ASSOCIATED WITH THE ROBINSON SCHOOL AND CONNECTION WITH WWTIP IS PART OF BASE BID.
- THE 1 1/2" PRESSURE SEWER SHALL FOLLOW ALIGNMENT OF EXISTING GRAVEL ROAD. THE EXACT LOCATION BE DETERMINED IN THE FIELD BY ARCHITECT AND APPROVED BY THE CONSERVATION COMMISSION.
- LIMIT OF WORK ALONG THE GRAVEL ROAD AND SEWER IS 20'-0" WIDE.
- INSTALL EROSION CONTROL ALONG GRAVEL ROAD SIMILAR TO THAT SHOWN ON DRAWING L-5 & L-6, PRIOR TO DOING ANY OTHER WORK.

**SITE UTILITY PLAN  
SHEET 2**

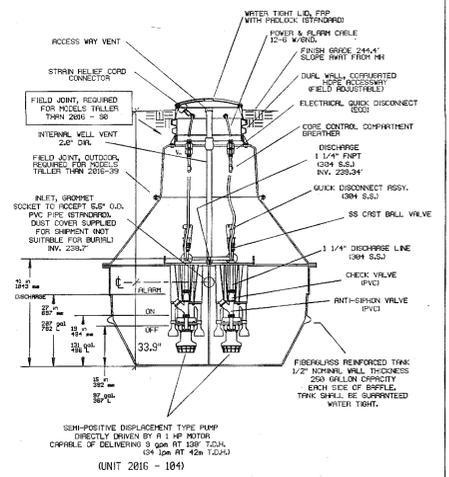
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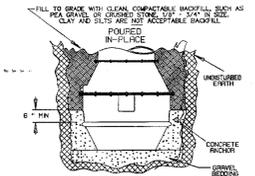


**DEMOLITION NOTES**  
ROBINSON SCHOOL SEWAGE DISPOSAL

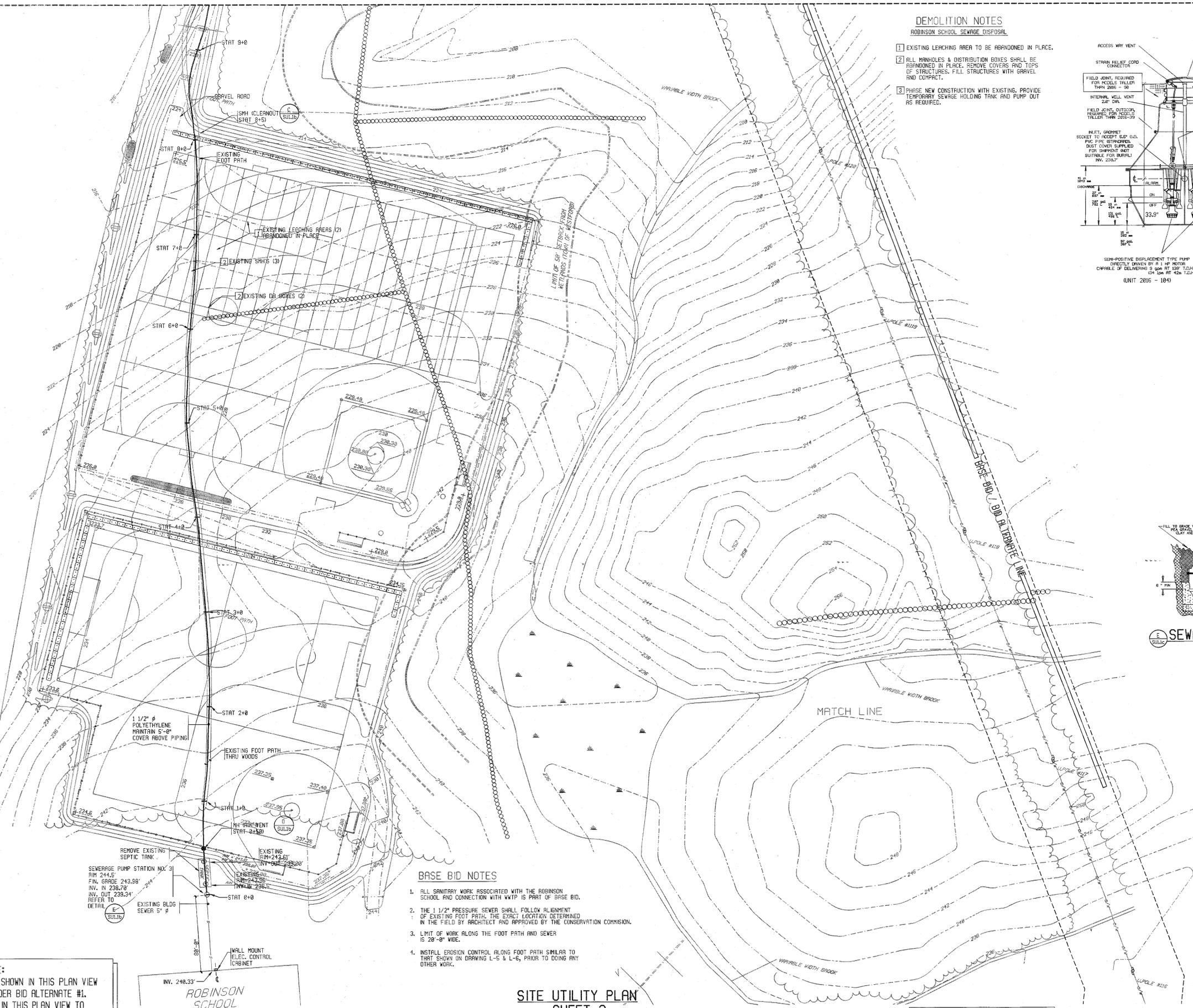
- 1) EXISTING LEACHING AREA TO BE ABANDONED IN PLACE.
- 2) ALL MANHOLES & DISTRIBUTION BOXES SHALL BE ABANDONED IN PLACE. REMOVE COVERS AND TOPS OF STRUCTURES. FILL STRUCTURES WITH GRAVEL AND COMPACT.
- 3) PHASE NEW CONSTRUCTION WITH EXISTING. PROVIDE TEMPORARY SEWAGE HOLDING TANK AND PUMP OUT AS REQUIRED.



UNIT 2016 - 184



**SEWAGE PUMP #3**  
NO SCALE



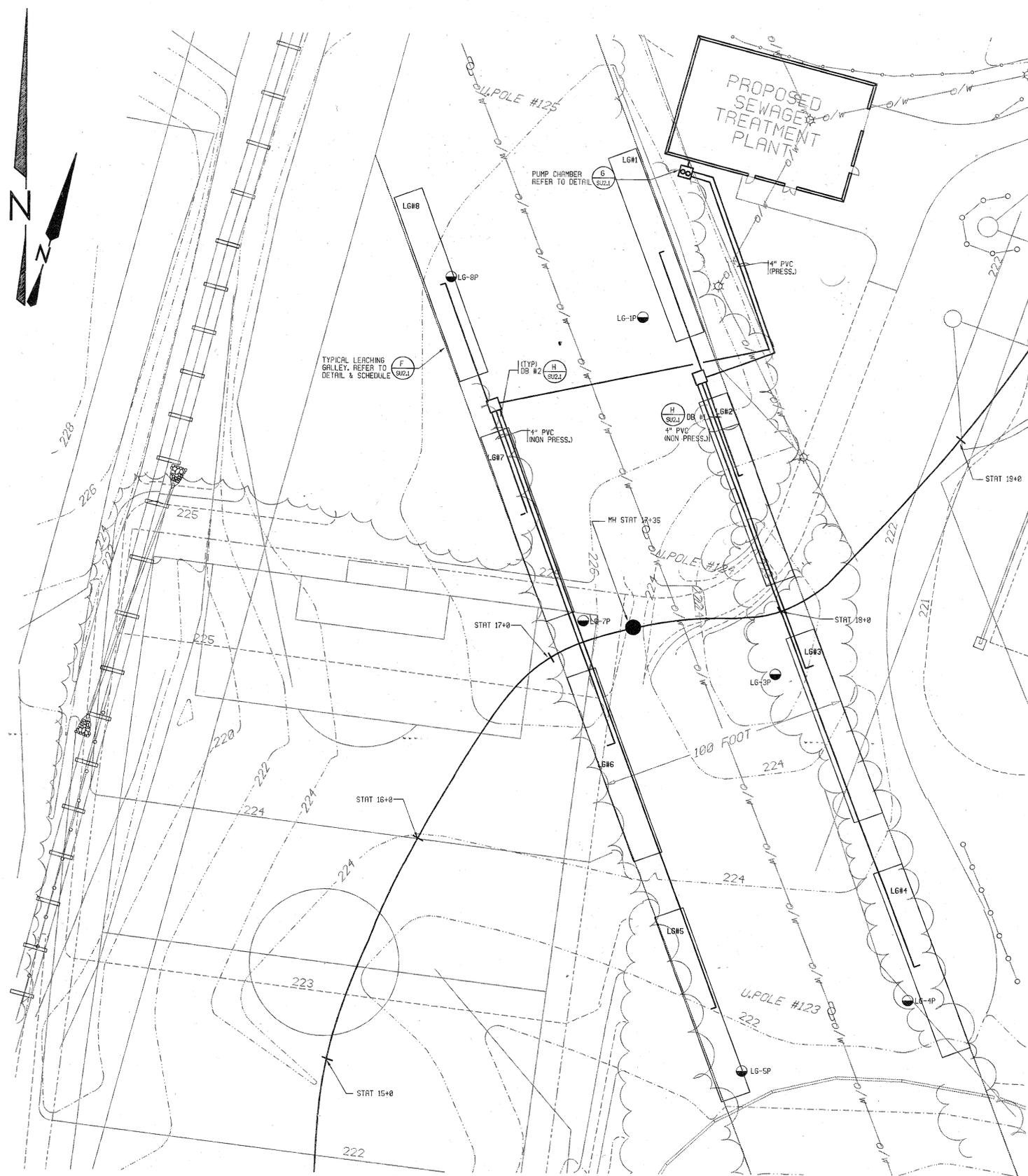
**BASE BID NOTES**

1. ALL SANITARY WORK ASSOCIATED WITH THE ROBINSON SCHOOL AND CONNECTION WITH WWTIP IS PART OF BASE BID.
2. THE 1 1/2" PRESSURE SEWER SHALL FOLLOW ALIGNMENT OF EXISTING FOOT PATH. THE EXACT LOCATION DETERMINED IN THE FIELD BY ARCHITECT AND APPROVED BY THE CONSERVATION COMMISSION.
3. LIMIT OF WORK ALONG THE FOOT PATH AND SEWER IS 20'-0" WIDE.
4. INSTALL EROSION CONTROL ALONG FOOT PATH SIMILAR TO THAT SHOWN ON DRAWING L-5 & L-6, PRIOR TO DOING ANY OTHER WORK.

**SITE UTILITY PLAN  
SHEET 3**  
SCALE: 1"=40'-0"

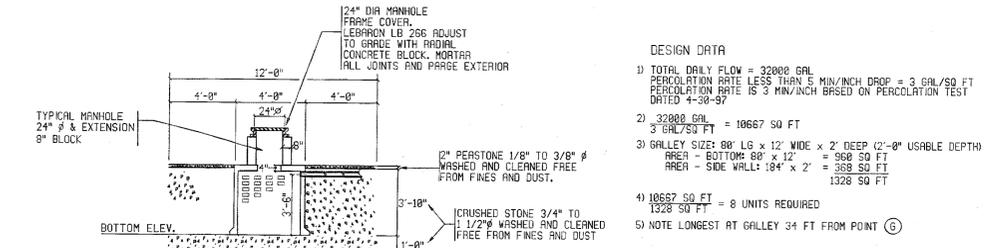
**NOTE:**  
WORK SHOWN IN THIS PLAN VIEW IS UNDER BID ALTERNATE #1. WORK IN THIS PLAN VIEW TO CONSTRUCT ENTIRE SANITARY SEWER SYSTEM IS IN BASE BID.

CONSTRUCTION OF NEW ATHLETIC FIELDS SHALL BE PART OF THE ADD ALTERNATE NO. 1. GRADES TO BE ADJUSTED ACCORDINGLY.

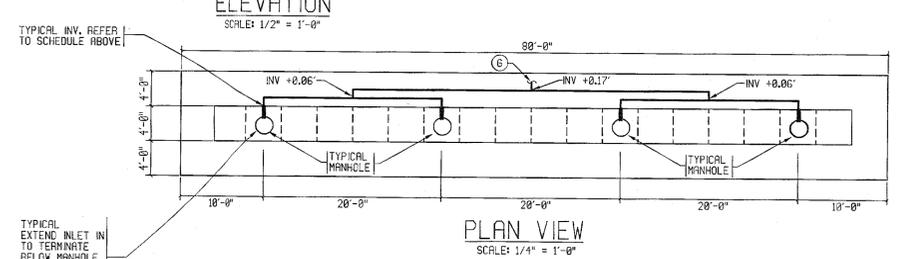


**LEACHING AREA PLAN**  
SCALE: 1" = 20'-0"

SITE EQUIPMENT SCHEDULE			
DISTRIBUTION BOX #1		DISTRIBUTION BOX #2	
FINISHED GRADE	226.8' ±	FINISHED GRADE	226.8' ±
INVERT IN	223.8'	INVERT IN	223.8'
INVERT OUT	222.8'	INVERT OUT	222.8'
LEACHING GALLEYS		LEACHING GALLEYS	
#1 FINISHED GRADE	226.8' ±	#5 FINISHED GRADE	222.0' ±
INVERT IN	222.1'	INVERT IN	218.1'
BOTTOM	218.8'	BOTTOM	214.8'
#2 FINISHED GRADE	224.0' ±	#6 FINISHED GRADE	224.0' ±
INVERT IN	218.5'	INVERT IN	218.5'
BOTTOM	216.07'	BOTTOM	216.07'
#3 FINISHED GRADE	224.0' ±	#7 FINISHED GRADE	226.8' ±
INVERT IN	219.5'	INVERT IN	222.1'
BOTTOM	216.07'	BOTTOM	218.8'
#4 FINISHED GRADE	224.0' ±	#8 FINISHED GRADE	226.8' ±
INVERT IN	219.8'	INVERT IN	222.1'
BOTTOM	216.07'	BOTTOM	218.8'

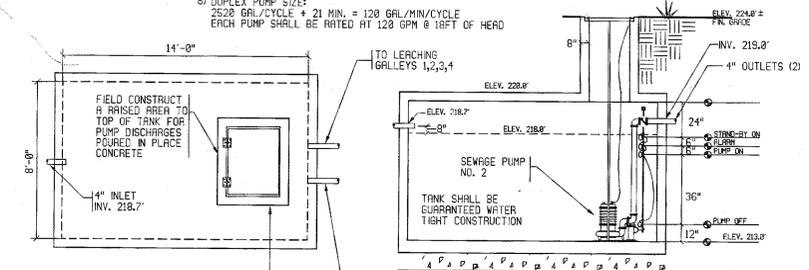


- DESIGN DATA**
- TOTAL DAILY FLOW = 32000 GAL  
PERCOLATION RATE LESS THAN 5 MIN/INCH DROP = 3 GAL/SQ FT  
PERCOLATION RATE IS 3 MIN/INCH BASED ON PERCOLATION TEST DATED 4-30-97
  - 32000 GAL = 10667 SQ FT  
3 GAL/SQ FT = 10667 SQ FT
  - GALLEY SIZE: 80' LG x 12' WIDE x 2' DEEP (2'-0\"/>

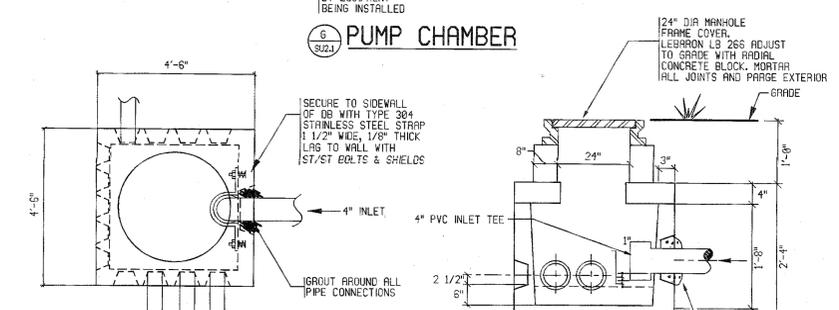


**LEACHING GALLEYS**  
SCALE: 1/4" = 1'-0"

- DESIGN DATA**
- DUPLEX PUMP SET SIZED TO DOSING HALF THE CHAMBERS AT A TIME WITH 1' OF COVERAGE
  - LEACHING CHAMBERS: 12' x 80' x 4' x .0833 FT x 7.5 GAL/CU FT = 2400 GALS.
  - DOSING TANK SIZE: 14 FT LONG x 8 FT x 3 FT DEEP DOWN x 7.5 GAL/CU FT = 2520 GAL/CYCLE. NET DEPTH OF COSE FOR (4) FOUR LEACHING CHAMBERS IS .0875 FT OR 1 1/16" INCH.
  - DESIGN FLOW = 32000 GAL/DAY  
DOSES PER DAY = 32000 GAL / 2520 GAL = 12.7 DOSES/DAY
  - ACTUAL DOSES PER DAY SHALL BE 6 DOSES/DAY OR 3 DOSES/SIDE. THIS IS PREDICATED ON ACTUAL WATER METER USAGE IN THE EXISTING SCHOOL.
  - DUPLEX PUMP SIZE: 2520 GAL/CYCLE x 21 MIN. = 120 GAL/MIN/CYCLE  
EACH PUMP SHALL BE RATED AT 120 GPM @ 18FT OF HEAD



**PUMP CHAMBER**  
SCALE: 1/4" = 1'-0"



**DISTRIBUTION BOX**  
SCALE: 1/2" = 1'-0"  
AS NOTED

**D·R·A**

DRUMMEY  
ROSENE  
ANDERSON  
INC.

Calby Hall  
141 Herrick Road  
P.O. Box 288  
Newton Centre, MA  
02459-0288

Architecture  
Interior Design

617-964-1780

**WESTFORD ACADEMY**

**TCTI THOMPSON CONSULTANTS, INC.**  
ENGINEERS

525 MILL ST.  
MARION, MA 02738  
608-748-2020 617-100-1003

**WESTFORD MASSACHUSETTS**

D.E.P. REVISIONS 10-17-97  
D.E.P. REVISIONS 8-28-97

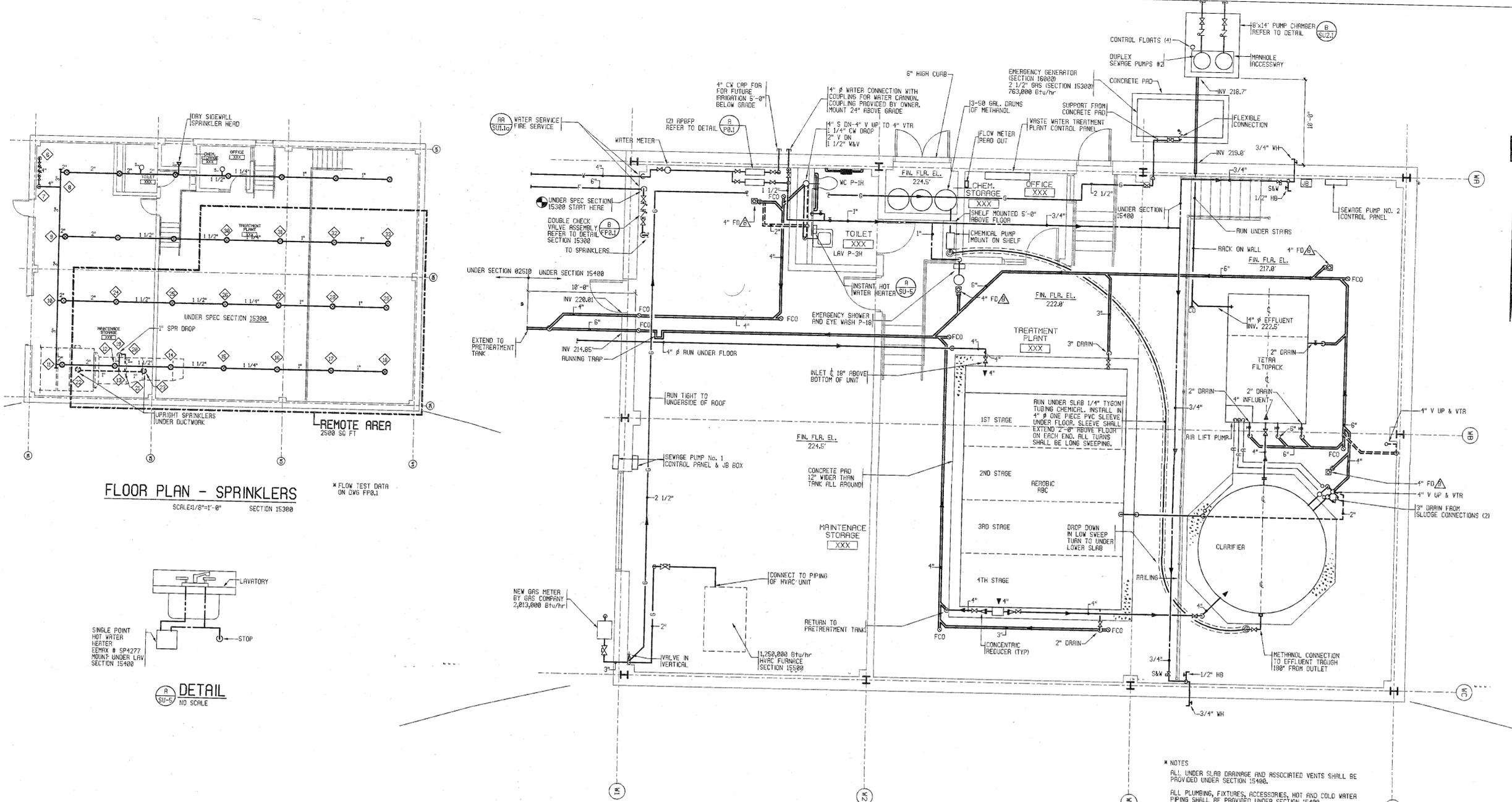


**SITE PLAN  
LEACHING AREA PLAN  
SITE UTILITIES**

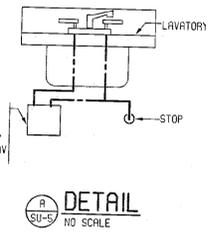
Scale: AS NOTED  
Dr. By: CST  
Job No.: 92-1836  
Date: 8/14/98

SU-4

**SU2.1**

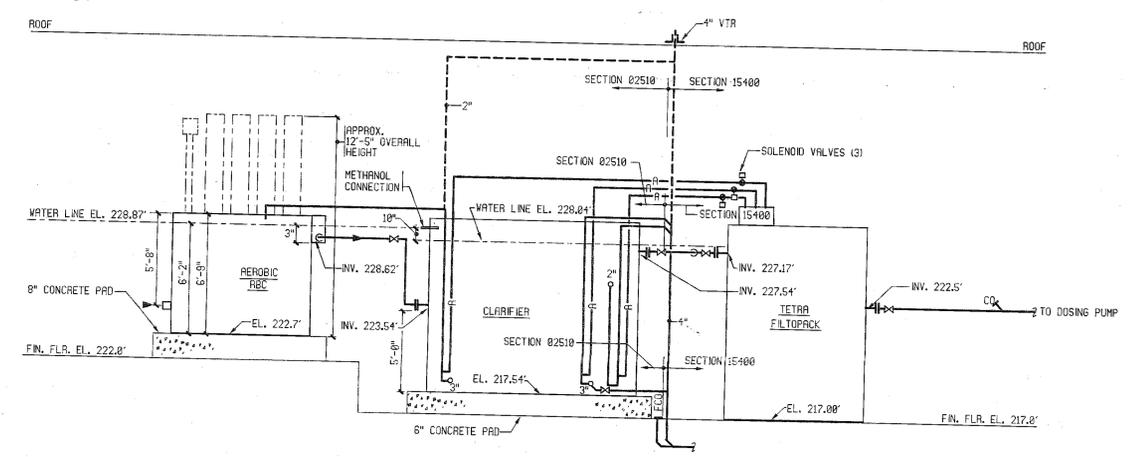


**FLOOR PLAN - SPRINKLERS**  
SCALE: 1/8"=1'-0" SECTION 15300



**WASTEWATER TREATMENT PLANT**  
SCALE: 1/4"=1'-0"

**\* NOTES**  
ALL UNDER SLAB DRAINAGE AND ASSOCIATED VENTS SHALL BE PROVIDED UNDER SECTION 15400.  
ALL PLUMBING, FIXTURES, ACCESSORIES, HOT AND COLD WATER PIPING SHALL BE PROVIDED UNDER SECTION 15400.  
ALL PROCESS WASTE WATER TREATMENT PLANT EQUIPMENT AND PIPING SHALL BE PROVIDED UNDER SECTION 02510.



**WASTEWATER TREATMENT SCHEMATIC**  
NO SCALE

**D·R·A**  
DRUMMEY  
ROSENE  
ANDERSON  
INC.  
Calby Hall  
141 Herrick Road  
P.O. Box 259  
Newton Centre, MA  
02459-0259

Architecture Interior Design 617-964-1768

**TCI THOMPSON CONSULTANTS, INC.**  
ENGINEERS  
525 MILL ST.  
MARION, MA 02738  
603-749-2620 603-749-4003

**WESTFORD ACADEMY**

**WESTFORD MASSACHUSETTS**

D.E.P. REVISIONS 10-17-97  
D.E.P. REVISIONS 8-28-97



**WASTEWATER TREATMENT PLANT FLOOR PLAN**

Scale: AS NOTED SU-5  
Dr. By: KJA  
Job No.: 92-193b  
Date: 01/14/98

**SU2.2**

# PRE-TREATMENT TANK 24,000 GAL

- DESIGN DATA**
- 1) WWP TOTAL DESIGN FLOW = 32000 GPD
  - 2) PRETREATMENT TANK 50% OF 32000 + 50% SLUDGE STORAGE
  - 3) 50% X 32,000 + 50% = 24,000 GALS.
  - 4) USE 1 - 24,000 GAL TANK EQUAL TO ROTONDA & SONS MODEL ST 8 X 10 - 24. STEEL REINFORCED PRE-CAST CONCRETE TANK DESIGN FOR H-20 LOADING.
  - 5) NO GARBAGE DISPOSAL TO BE USED
  - 6) WEIGHT OF TANK = 180,500 LBS.

### BUOYANCY CALCULATION

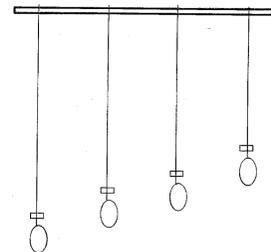
24,000 GALLON TANK	16' x 11' x 9' DEEP
24,000 GALLON TANK	180,500 LBS.
7'-0" EARTH COVER	630 P.S.F.
GROUND WATER LEVEL	204.0' ELEVATION
BOTTOM OF TANK	205.0' ELEVATION
ALLOW AN ADDITION 3' G.W.	207.0' ELEVATION
HYDROSTATIC UP LIFT 2 (62.5)	125 P.S.F.
TANK (EMPTY) = 180,500 LBS	= 317 P.S.F.
EARTH COVER = 46 x 11	= 630 P.S.F.
TOTAL	= 947 P.S.F.
FACTOR OF SAFETY = $\frac{947}{125}$	= 7.58

# EQUALIZATION TANK 18,000 GAL

- DESIGN DATA**
- 1) WWP TOTAL DESIGN FLOW = 32000 GPD
  - 2) EQUALIZATION TANK 50% OF 32000 GPD
  - 3) 50% X 32000 GAL/DAY = 16000 GALS.
  - 4) BOTTOM OF TANK TO BE SLOPE 2% MIN. WE HAVE SHOWN 3.3% SLOPE.
  - 5) USE 1 - 18000 GALLON TANK EQUAL TO ROTONDA & SONS MODEL # 57 8 X 10 STEEL REINFORCED PRECAST CONCRETE TANK DESIGNED FOR H-20 LOADING.
  - 6) NO GARBAGE DISPOSAL TO BE USED
  - 7) SLOPE AREA = 10' X 30' X 1' X 7.5 GAL = 1125
  - NET VOLUME 18,000 - 1125 = 16,875 GAL
  - 8) PUMPS SHALL BE VEIL PUMP CO. GRINDER TYPE RATED AT 100 GPM @ 26 FT HEAD W/ 1 HP MOTORS, MODEL 2516 (REFER TO SPECS FOR DETAILS)
  - 9) WEIGHT OF TANK = 128,200 LBS.

### BUOYANCY CALCULATION

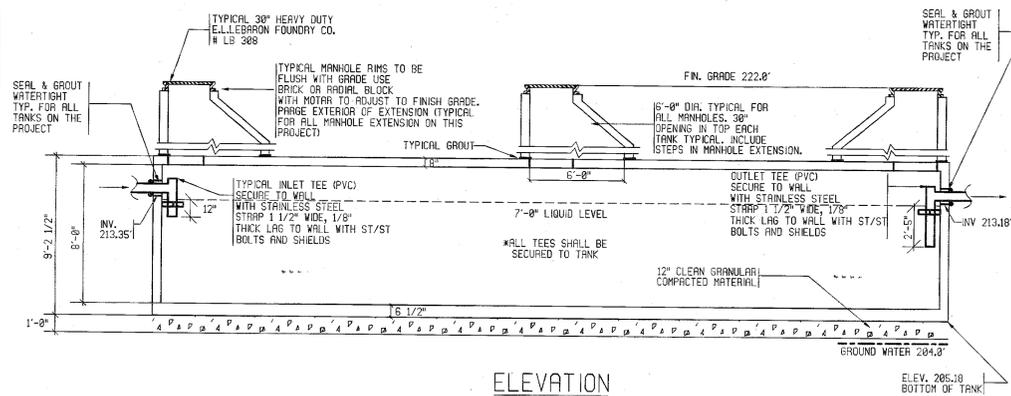
18,000 GALLON TANK	35' x 11' x 9' DEEP
18,000 GALLON TANK	128,200 LBS.
7'-0" EARTH COVER	630 P.S.F.
GROUND WATER LEVEL	204.0' ELEVATION
BOTTOM OF TANK	205.0' ELEVATION
ALLOW AN ADDITION 3' G.W.	207.0' ELEVATION
HYDROSTATIC UP LIFT 2 (62.5)	125 P.S.F.
TANK (EMPTY) = 128,200 LBS	= 333 P.S.F.
EARTH COVER = 35 x 11	= 630 P.S.F.
TOTAL	= 963 P.S.F.
FACTOR OF SAFETY = $\frac{963}{125}$	= 7.70



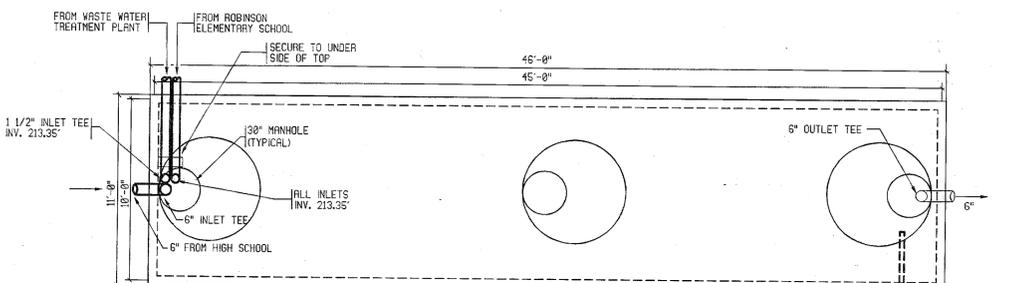
PUMP FLOAT ASSEMBLY  
NO SCALE

# GREASE TRAP

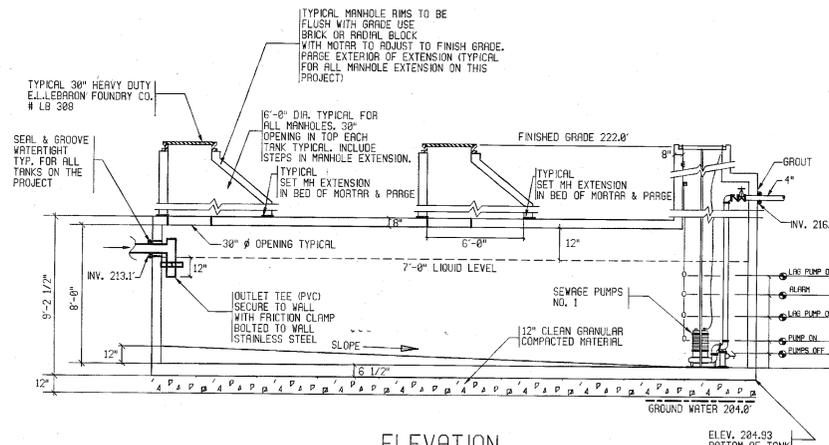
- DESIGN DATA**
- 1) KITCHEN GREASE TRAP - 1738 STUDENT, 4 GPD PER STUDENT.
  - 2) 1738 X 4 = 6952 GALLONS USE 7000 GALLON
  - 3) USE 1 - 7000 GALLON TANK EQUAL TO ROTONDA & SONS MODEL # ST 9 X 16 - 7 STEEL REINFORCED PRECAST CONCRETE TANK DESIGNED FOR H-20 LOADING.
  - 4) NO GARBAGE DISPOSAL TO BE USED



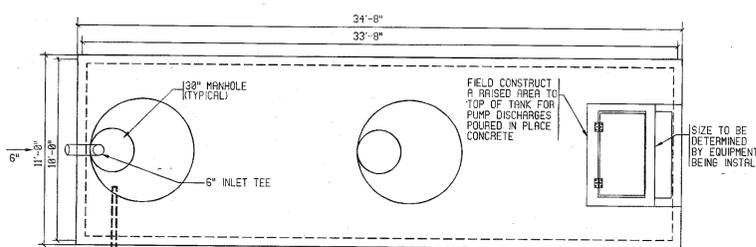
ELEVATION  
SCALE: 1/4" = 1'-0"



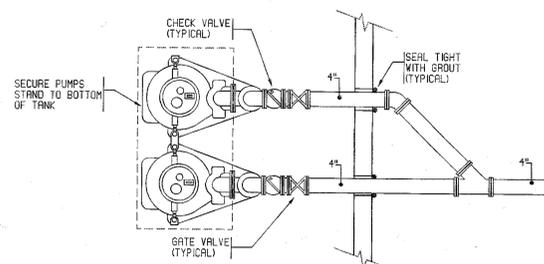
PLAN VIEW  
SCALE: 1/4" = 1'-0"



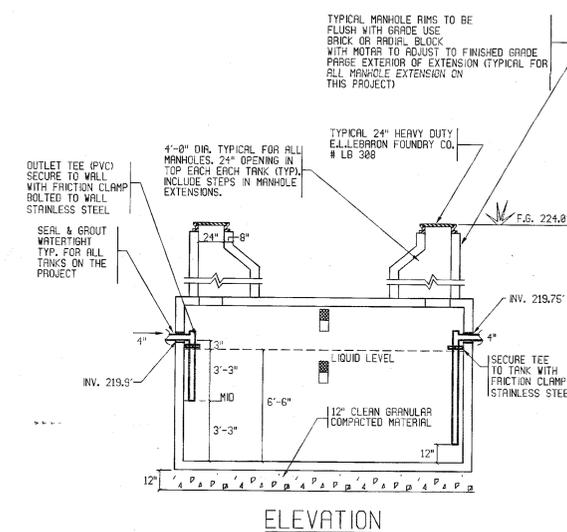
ELEVATION  
SCALE: 1/4" = 1'-0"



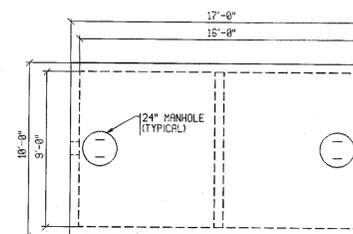
PLAN VIEW  
SCALE: 1/4" = 1'-0"



PUMP PLAN VIEW  
NOT TO SCALE



ELEVATION  
SCALE: 1/4" = 1'-0"



PLAN VIEW  
SCALE: 1/4" = 1'-0"

### NOTES:

STRUCTURES (TANKS) SHOWN ON THIS DRAWING SHALL BE GUARANTEED WATER TIGHT. INSTALLATION METHODS SHALL FOLLOW MANUFACTURERS RECOMMENDATIONS. ADDITIONAL REQUIREMENTS ARE AS FOLLOWS:

- 1) THE BASE MUST BE A TRANSIT LEVELED CLEAN GRANULAR COMPACTED MATERIAL TO SUPPORT THE CHAMBER WITHOUT THE CHANCE OF DIFFERENTIAL SETTLEMENT.
- 2) THE EXCAVATION MUST BE PUMPED AND KEPT DRY DURING INSTALLATION.
- 3) THE CHAMBER MUST BE BACKFILLED WITHIN 24 HOURS OF THE INSTALLATION, STARTING WITH THE MIDDLE OF THE TANK.
- 4) THE CRANE (OBTAINED BY CONTRACTOR) MUST BE LARGE ENOUGH TO PLACE THE SECTIONS WITHOUT DAMAGING THEM IN ANY WAY.
- 5) SUITABLE BACKFILL MATERIAL AND PLACEMENT METHODS MUST BE USED TO AVOID ANY DAMAGE OR SHIFTING OF THE SECTIONS.
- 6) THE JOINTS MUST BE KEPT CLEAN OF ANY FOREIGN MATERIALS WHILE THE SECTIONS ARE BEING DRAWN TOGETHER.
- 7) IN CASE OF HOLDING TANKS, PLEASE IDENTIFY ANY UNUSUAL COMPONENTS OF LIQUID RETAINED AT TIME OF ORDER (CERTAIN CHEMICALS REACT ADVERSELY WITH THE GASKET MATERIAL.)
- 8) TANK MUST BE BACKFILLED PRIOR TO FILLING (WATER TESTING) TO PREVENT POTENTIAL JOINT SEPARATION.

**D.R.A.**

DRUMMEY  
ROSEANE  
ANDERSON  
INC.

Colby Hall  
141 Merrick Road  
P.O. Box 289  
Newton Centre, MA  
02459-0289

Architecture  
Interior Design

617-961-1780

# WESTFORD ACADEMY

# WESTFORD MASSACHUSETTS

D.E.P. REVISIONS 10-17-97  
D.E.P. REVISIONS 8-28-97



# SITE PLAN DETAILS SITE UTILITIES

Scale: AS NOTED  
Dr. By: CST  
Job No.: 92-183b  
Date: 01/14/98

SU3.1

# AEROBIC RBC

## DESIGN DATA

WASTEWATER INFLUENT CHARACTERISTICS

AVERAGE FLOW (Q <sub>AV</sub> )	.832 MGD
PEAK DAILY FLOW (Q <sub>P</sub> )	.84 MGD
MINIMUM FLOW (Q <sub>M</sub> )	.803 MGD
TOTAL BOD (Q <sub>T</sub> )	250 MG/L
SOLUBLE BOD (F <sub>1</sub> )	150 MG/L
SUSP. SOLIDS (S <sub>1</sub> )	250 MG/L
NH <sub>3</sub> -N (ND)	45 MG/L
WATER TEMP (T <sub>1</sub> )	55 DEG F

WASTEWATER EFFLUENT REQUIREMENTS

EFF TOTAL BOD (Q <sub>2</sub> )	30 MG/L
EFF SOL BOD (F <sub>2</sub> )	15 MG/L
EFF SUSP.SOLIDS (S <sub>2</sub> )	30 MG/L
EFF NH <sub>3</sub> -N (NS)	2 MG/L

\*EFF SOL BOD SPECIFIED AS 15. HOWEVER BOD PHASE IS DESIGNED TO REDUCE BOD CONCENTRATION TO 15 OR TO NH<sub>3</sub> INFLUENT CONCENTRATION WHICHEVER IS LEAST. ADDITIONAL BOD REDUCTION IN NH<sub>3</sub> REMOVAL PHASE.

# CLARIFIER

## DESIGN DATA

- 300 GPD / SQ FT
- 32000 GPD TOTAL FLOW  
32000 DIVIDED BY 300 = 107 SQ FT REQUIRED.
- 12 FT DIA CLARIFY  
π x R<sup>2</sup> = A  
3.14 x 6x6 = 113 SQ FT

# TETRA FILTOPACK FILTER

## DESIGN DATA

GENERAL DESIGN PARAMETERS:

MEDIA DEPTH	= 4.0 FEET
REACTOR VOLUME VOID FACTOR	= 0.4
REACTOR SURFACE AREA	= 12.5 SQ FT, FILTOPACK CELL
INITIAL BW WATER RATE	= 5 GPM/SQ FT
INITIAL BW WATER DURATION	= 15 MINUTES
FINAL BW WATER RATE	= 5 GPM/SQ FT
FINAL BW WATER DURATION	= 5 MINUTES
BW AIR RATE	= 3 LCFM/SQ FT
METHANOL STORAGE TANKS	= 55 GAL. (TOTAL) (2)

INFLUENT CHARACTERISTICS:

PARAMETER	SUMMER	WINTER
NITRATE AS N, MG/L @ ADF	= 30.0	30.0
NITRATE AS N, MG/L @ PK-DRY	= 30.0	30.0
TSS, MG/L @ ADF	= 30.0	30.0
PHOSPHATE AS P, MG/L @ ADF	= 2.0	2.0
pH, SU	= 7.0	7.0
DO, MG/L	= 2.0	2.0
MIN. TEMPERATURE, DEG. C	= 20.0	12.8

FLOW:

	SUMMER	WINTER
ADF, MGD	= 0.832	0.832
GPM	= 22	22
PEAK-DAY, MGD	= 0.832	0.832
GPM	= 22	22
PEAK-HOUR, MGD	= 0.832	0.832
GPM	= 22	22

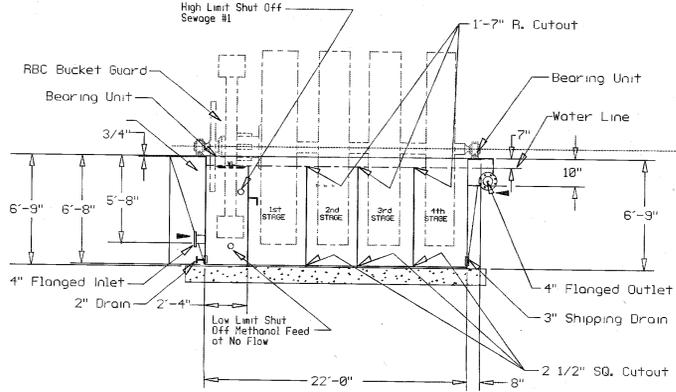
DESIRED EFFLUENT CHARACTERISTICS (DISCHARGE LIMITS):

PARAMETER	SUMMER	WINTER
NITRATE AS N, MG/L @ ADF	= 2.0	2.0
NITRATE AS N, MG/L @ PK-DRY	= 2.0	2.0
TSS, MG/L	= 5.0	5.0
pH, SU	= 6-9	6-9

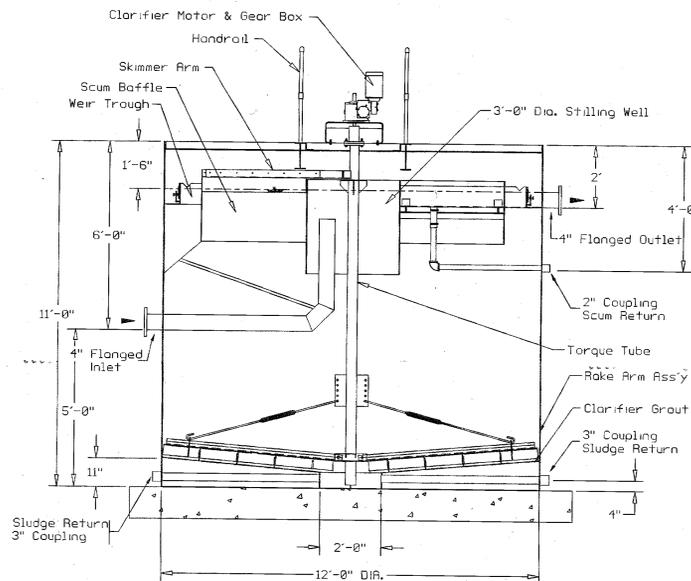
HYDRAULIC LIMITS:

FILTR. RATE @ ADF W/ALL IS	= 5.0 GPM/SQ FT
FILTR. RATE @ ADF W/1 OOS	= 6PM/SQ FT
FILTR. RATE @ PK W/ALL IS	= 5.0 GPM/SQ FT
FILTR. RATE @ PK W/1 OOS	= 6PM/SQ FT

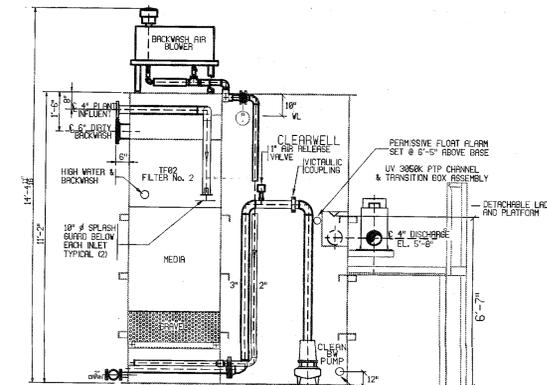
CLEARWELL GROSS VOLUME = 1740 GAL  
NET USEABLE VOLUME = 1400 GAL  
BACK WASH USE = 1250 GAL



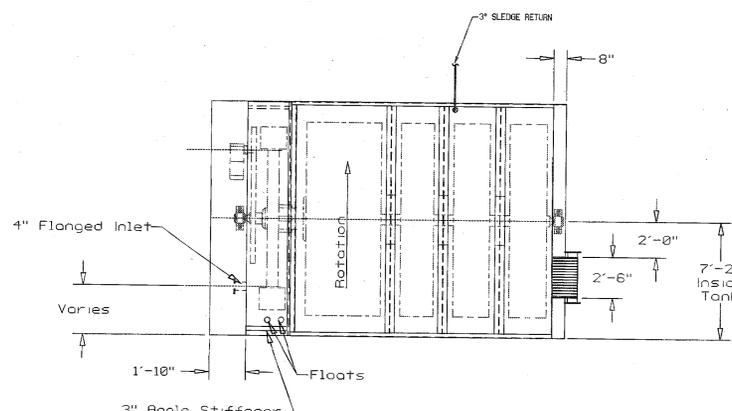
ELEVATION  
NOT TO SCALE



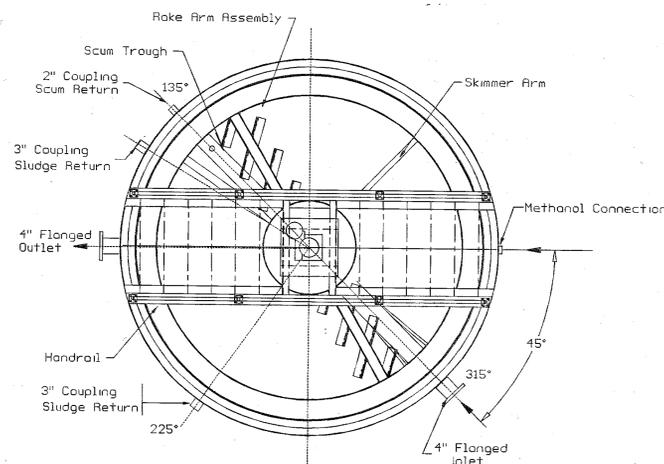
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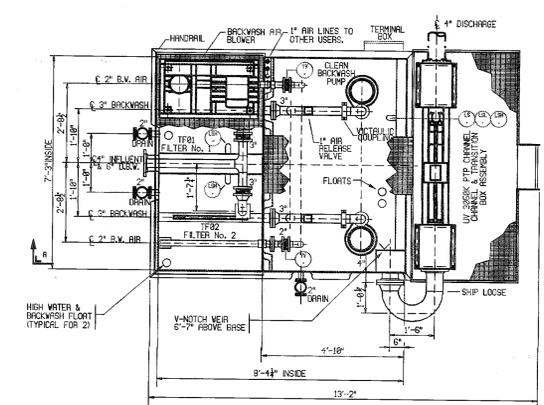
ELEVATION  
NOT TO SCALE



PLAN VIEW  
NOT TO SCALE



PLAN VIEW  
NOT TO SCALE



PLAN VIEW  
NOT TO SCALE

**D·R·A**

DRUMMEY ROSEANE ANDERSON INC.  
Colby Hall  
141 Herrick Road  
P.O. Box 299  
Newton Centre, MA  
02459-0299

Architecture Interior Design 617-964-1700

# WESTFORD ACADEMY

# WESTFORD MASSACHUSETTS

D.E.P. REVISION 10-17-97  
D.E.P. REVISION 8-28-97



# WASTEWATER TREATMENT PLANT DETAILS

Scale: AS NOTED SU-7  
Dr. By: WJA  
Job No.: 92-183b  
Date: 01/14/98

SU3.2

**SITE SUITABILITY ASSESSMENT FOR ON SITE SEWAGE DISPOSAL**

PERFORMED BY: MICHAEL J. HICKEY P.E. CERTIFICATION NUMBER: MA PE NO. 27564  
WITNESSED BY: MARGO WEBER - DEP  
KEVIN JOHNSTON - WESTFORD BOARD OF HEALTH

LOCATION ADDRESS OR LOT NUMBER: 30 PATTEN ROAD WESTFORD, MA 01886	OWNER'S NAME, ADDRESS AND TEL. # TOWN OF WESTFORD WESTFORD SCHOOL COMMITTEE 35 TOWN FARM ROAD WESTFORD, MA 01886 (508) 692-5563
---	--

NEW CONSTRUCTION  REPAIR

**ON-SITE REVIEW**

DEEP HOLE NUMBER: LG-3P DATE: 4/30/97 TIME: 12:40 PM WEATHER: CLEAR  
LOCATION (Identify on site plan): EASEMENT SOUTH OF TRACK, BETWEEN POLES 123 & 125  
LAND USE: UTILITY EASEMENT SLOPE (X): 2 SURFACE STONE: <10%  
VEGETATION: GRASS & SCRUB BRUSH  
LANDFORM: OUTWASH PLAIN  
DISTANCES FROM:  
OPEN WATER BODY: 500 feet DRAINAGEWAY: >500 feet  
POSSIBLE WET AREA: 280 feet PROPERTY LINE: 300 feet  
DRINKING WATER WELL: ----- OTHER: -----

Depth from Surface (inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)
0-9	A				
9-25	B	SANDY LOAM			
25-59	C <sub>1</sub>	SAND	2.5Y 8/3	NONE	
59-144	C <sub>2</sub>	SAND	2.5Y 8/3	NONE	
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PARENT MATERIAL (geologic): GLACIAL OUTWASH DEPTH OF BEDROCK: ---  
DEPTH OF GROUND WATER: STANDING WATER IN HOLE: NONE WEEPING FROM PIT FACE: NONE  
ESTIMATED SEASONAL HIGH GROUND WATER: BELOW 12'-0"

**ON-SITE REVIEW**

DEEP HOLE NUMBER: LG-1P DATE: 4/30/97 TIME: --- WEATHER: CLEAR  
LOCATION (Identify on site plan): EASEMENT SOUTH OF TRACK, BETWEEN POLES 123 & 125  
LAND USE: UTILITY EASEMENT SLOPE (X): 2 SURFACE STONE: <10%  
VEGETATION: GRASS & SCRUB BRUSH  
LANDFORM: OUTWASH PLAIN  
DISTANCES FROM:  
OPEN WATER BODY: 600 feet DRAINAGEWAY: >500 feet  
POSSIBLE WET AREA: 460 feet PROPERTY LINE: 190 feet  
DRINKING WATER WELL: ----- OTHER: -----

Depth from Surface (inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)
0-14	A				
14-28	B	SANDY LOAM			
28-62	C <sub>1</sub>	SAND	2.5Y 5/4	NONE	
62-76	C <sub>2</sub>	FINE SAND	2.5Y 5/3	NONE	
76-88	C <sub>3</sub>	SANDY LOAM	2.5Y 6/4	NONE	
88-144	C <sub>4</sub>	FINE SAND	2.5Y 5/3	NONE	
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PARENT MATERIAL (geologic): GLACIAL OUTWASH DEPTH OF BEDROCK: ---  
DEPTH OF GROUND WATER: STANDING WATER IN HOLE: NONE WEEPING FROM PIT FACE: NONE  
ESTIMATED SEASONAL HIGH GROUND WATER: BELOW 12'-0"

**ON-SITE REVIEW**

DEEP HOLE NUMBER: LG-4P DATE: 4/30/97 TIME: 10:24 AM WEATHER: CLEAR  
LOCATION (Identify on site plan): EASEMENT SOUTH OF TRACK, BETWEEN POLES 123 & 125  
LAND USE: UTILITY EASEMENT SLOPE (X): 2 SURFACE STONE: <10%  
VEGETATION: GRASS & SCRUB BRUSH  
LANDFORM: OUTWASH PLAIN  
DISTANCES FROM:  
OPEN WATER BODY: 440 feet DRAINAGEWAY: >500 feet  
POSSIBLE WET AREA: 145 feet PROPERTY LINE: 380 feet  
DRINKING WATER WELL: ----- OTHER: -----

Depth from Surface (inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)
0-15	A				
15-31	B	SANDY LOAM			
31-43	C <sub>1</sub>	SAND	2.5Y 5/3	NONE	
43-54	C <sub>2</sub>	LOAMY SAND	2.5Y 6/3	NONE	
54-95	C <sub>3</sub>	LOAMY SAND	2.5Y 6/3	NONE	
95-111	C <sub>4</sub>	LOAMY SAND			EXCAVATION UNSTABLE
111-141	C <sub>5</sub>	LOAMY SAND			BELOW THIS POINT
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PARENT MATERIAL (geologic): GLACIAL OUTWASH DEPTH OF BEDROCK: ---  
DEPTH OF GROUND WATER: STANDING WATER IN HOLE: NONE WEEPING FROM PIT FACE: NONE  
ESTIMATED SEASONAL HIGH GROUND WATER: BELOW 12'-0"

**OFFICE REVIEW**

PUBLISHED SOIL SURVEY AVAILABLE: NO  YES   
YEAR PUBLISHED: 1995 PUBLICATION SCALE: 1:25,000 SOIL MAP UNIT: #20  
DRAINAGE CLASS: EXCESSIVE SOIL LIMITATIONS: DROUGHT  
SURFICIAL GEOLOGIC REPORTS AVAILABLE: NO  YES   
YEAR PUBLISHED: --- PUBLICATION SCALE: ---  
GEOLOGIC MATERIAL MAP UNIT: ---  
LANDFORM: ---  
FLOOD INSURANCE MAP:  
ABOVE 500 YEAR FLOOD BOUNDARY NO  YES   
WITHIN 500 YEAR FLOOD BOUNDARY NO  YES   
WITHIN 100 YEAR FLOOD BOUNDARY NO  YES

**ON-SITE REVIEW**

DEEP HOLE NUMBER: LG-5P DATE: 4/30/97 TIME: 9:26 AM WEATHER: CLEAR  
LOCATION (Identify on site plan): EASEMENT SOUTH OF TRACK, BETWEEN POLES 123 & 125  
LAND USE: UTILITY EASEMENT SLOPE (X): 2 SURFACE STONE: <10%  
VEGETATION: GRASS & SCRUB BRUSH  
LANDFORM: OUTWASH PLAIN  
DISTANCES FROM:  
OPEN WATER BODY: 480 feet DRAINAGEWAY: >500 feet  
POSSIBLE WET AREA: 125 feet PROPERTY LINE: 320 feet  
DRINKING WATER WELL: ----- OTHER: -----

Depth from Surface (inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)
0-9	A				
9-21	B	SANDY LOAM	10YR 5/8	NONE	
21-96	C <sub>1</sub>	LOAMY SAND	2.5Y 7/3	NONE	
96-158	C <sub>2</sub>	SAND	2.5Y 6/3	NONE	
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PARENT MATERIAL (geologic): GLACIAL OUTWASH DEPTH OF BEDROCK: ---  
DEPTH OF GROUND WATER: STANDING WATER IN HOLE: NONE WEEPING FROM PIT FACE: NONE  
ESTIMATED SEASONAL HIGH GROUND WATER: BELOW 12'-0"

**ON-SITE REVIEW**

DEEP HOLE NUMBER: LG-7P DATE: 4/30/97 TIME: --- WEATHER: CLEAR  
LOCATION (Identify on site plan): EASEMENT SOUTH OF TRACK, BETWEEN POLES 123 & 125  
LAND USE: UTILITY EASEMENT SLOPE (X): 2 SURFACE STONE: <10%  
VEGETATION: GRASS & SCRUB BRUSH  
LANDFORM: OUTWASH PLAIN  
DISTANCES FROM:  
OPEN WATER BODY: 620 feet DRAINAGEWAY: >500 feet  
POSSIBLE WET AREA: 320 feet PROPERTY LINE: 200 feet  
DRINKING WATER WELL: ----- OTHER: -----

Depth from Surface (inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)
0-12	A				
12-36	B				
36-72	C <sub>1</sub>	SAND	2.5Y 5/4	NONE	
72-112	C <sub>2</sub>	LOAMY SAND	2.5Y 6/3	NONE	
112-144	C <sub>3</sub>	SAND	2.5Y 7/3	NONE	
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PARENT MATERIAL (geologic): GLACIAL OUTWASH DEPTH OF BEDROCK: ---  
DEPTH OF GROUND WATER: STANDING WATER IN HOLE: NONE WEEPING FROM PIT FACE: NONE  
ESTIMATED SEASONAL HIGH GROUND WATER: BELOW 12'-0"

**ON-SITE REVIEW**

DEEP HOLE NUMBER: LG-8P DATE: 4/30/97 TIME: 12:20 PM WEATHER: CLEAR  
LOCATION (Identify on site plan): EASEMENT SOUTH OF TRACK, BETWEEN POLES 123 & 125  
LAND USE: UTILITY EASEMENT SLOPE (X): 2 SURFACE STONE: <10%  
VEGETATION: GRASS & SCRUB BRUSH  
LANDFORM: OUTWASH PLAIN  
DISTANCES FROM:  
OPEN WATER BODY: 720 feet DRAINAGEWAY: >500 feet  
POSSIBLE WET AREA: 440 feet PROPERTY LINE: 130 feet  
DRINKING WATER WELL: ----- OTHER: -----

Depth from Surface (inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)
0-7	A				
7-28	B				
28-62	C <sub>1</sub>	COURSE SAND	2.5Y 5/3	NONE	
62-132	C <sub>2</sub>	FINE SAND	2.5Y 6/4	NONE	
---	---	---	---	---	---
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PARENT MATERIAL (geologic): GLACIAL OUTWASH DEPTH OF BEDROCK: ---  
DEPTH OF GROUND WATER: STANDING WATER IN HOLE: NONE WEEPING FROM PIT FACE: NONE  
ESTIMATED SEASONAL HIGH GROUND WATER: BELOW 11'-0"

**WETLAND AREA:**

NATIONAL WETLAND INVENTORY MAP (MAP UNIT):  
WETLANDS CONSERVANCY PROGRAM MAP (MAP UNIT):  
CURRENT WATER RESOURCE CONDITIONS (USGS): MONTH  
RANGE: ABOVE NORMAL  NORMAL  BELOW NORMAL   
OTHER REFERENCES REVIEWED:

**DETERMINATION OF SEASONAL HIGH WATER TABLE**

METHOD USED:  
 DEPTH OBSERVED STANDING IN OBSERVATION HOLE: >144 inches NONE OBSERVED  
 DEPTH WEEPING FROM SIDE OF OBSERVATION HOLE:  
 DEPTH OF SOIL MOTTLES: NONE OBSERVED  
 GROUND WATER ADJUSTMENT:

INDEX WELL NUMBER: --- READING DATE: --- INDEX WELL LEVEL: ---  
ADJUSTMENT FACTOR: --- ADJUSTED GROUND WATER LEVEL: ---

DATE: 4/30/97	TIME: ---	
OBSERVATION HOLE#	LG7P	LG8P
DEPTH OF PERC	72"	64"
START PRE-SORK	12:39 PM	11:25 AM
END PRE SORK	12:54 PM	UNABLE TO SORK HOLE
TIME AT 12"	24 GALLONS	UNABLE TO SORK HOLE
TIME AT 9"	RODED, UNABLE TO SORK	24 GALLONS
TIME AT 6"	UNABLE TO SORK	RODED
TIME (9"-6")	---	---
RATE MIN./INCH	<2 MIN./ INCH	<2 MIN./ INCH

SITE SUITABILITY ASSESSMENT:  SITE PASSED  SITE FAILED  
ADDITIONAL TESTING NEEDED:  
PERFORMED BY: MICHAEL J. HICKEY PE CERTIFICATION NUMBER: 27564  
WITNESSED BY: MARGO WEBER - DEP  
KEVIN JOHNSTON - WESTFORD BOARD OF HEALTH  
COMMENTS:

**DETERMINATION OF SEASONAL HIGH WATER TABLE**

METHOD USED:  
 DEPTH OBSERVED STANDING IN OBSERVATION HOLE: >144 inches NONE OBSERVED  
 DEPTH WEEPING FROM SIDE OF OBSERVATION HOLE:  
 DEPTH OF SOIL MOTTLES: NONE OBSERVED  
 GROUND WATER ADJUSTMENT:

INDEX WELL NUMBER: --- READING DATE: --- INDEX WELL LEVEL: ---  
ADJUSTMENT FACTOR: --- ADJUSTED GROUND WATER LEVEL: ---

DATE: 4/30/97	TIME: ---	
OBSERVATION HOLE#	LG4P	LG5P
DEPTH OF PERC	72"	53"
START PRE-SORK	10:45 AM	9:44 AM
END PRE SORK	11:00 AM	9:58 AM
TIME AT 12"	11:00 AM	9:59 AM
TIME AT 9"	11:06 AM	10:06 AM
TIME AT 6"	11:14 AM	10:16 AM
TIME (9"-6")	8 MIN	10 MIN
RATE MIN./INCH	2.67 MIN./ INCH	3.3 MIN./ INCH

SITE SUITABILITY ASSESSMENT:  SITE PASSED  SITE FAILED  
ADDITIONAL TESTING NEEDED:  
PERFORMED BY: MICHAEL J. HICKEY PE CERTIFICATION NUMBER: 27564  
WITNESSED BY: MARGO WEBER - DEP  
KEVIN JOHNSTON - WESTFORD BOARD OF HEALTH  
COMMENTS:

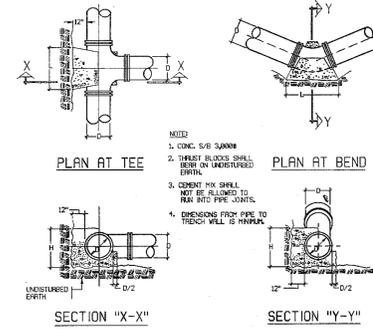
**DETERMINATION OF SEASONAL HIGH WATER TABLE**

METHOD USED:  
 DEPTH OBSERVED STANDING IN OBSERVATION HOLE: >144 inches NONE OBSERVED  
 DEPTH WEEPING FROM SIDE OF OBSERVATION HOLE:  
 DEPTH OF SOIL MOTTLES: NONE OBSERVED  
 GROUND WATER ADJUSTMENT:

INDEX WELL NUMBER: --- READING DATE: --- INDEX WELL LEVEL: ---  
ADJUSTMENT FACTOR: --- ADJUSTED GROUND WATER LEVEL: ---

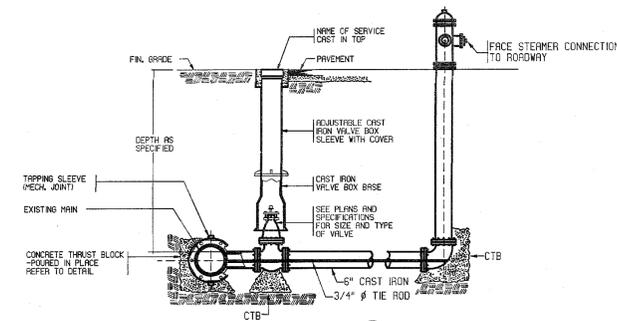
DATE: 4/30/97	TIME: ---	
OBSERVATION HOLE#	LG7P	LG8P
DEPTH OF PERC	72"	64"
START PRE-SORK	UNABLE TO SORK HOLE	UNABLE TO SORK HOLE
END PRE SORK	UNABLE TO SORK HOLE	UNABLE TO SORK HOLE
TIME AT 12"	---	---
TIME AT 9"	---	---
TIME AT 6"	---	---
TIME (9"-6")	---	---
RATE MIN./INCH	2 MIN./ INCH	2 MIN./ INCH

SITE SUITABILITY ASSESSMENT:  SITE PASSED  SITE FAILED  
ADDITIONAL TESTING NEEDED:  
PERFORMED BY: MICHAEL J. HICKEY PE CERTIFICATION NUMBER: 27564  
WITNESSED BY: MARGO WEBER - DEP  
KEVIN JOHNSTON - WESTFORD BOARD OF HEALTH  
COMMENTS:

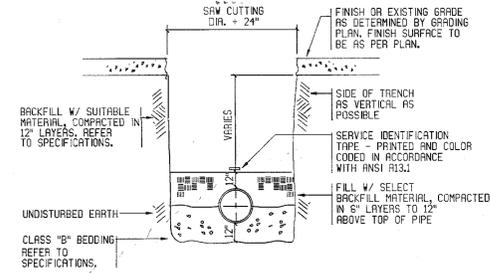


DIMENSION	1/4" BEND	1/2" BEND	3/4" BEND	1" BEND
D	4"	6"	8"	10"
H	4"	6"	8"	10"
L	12"	12"	12"	12"
M	4"	6"	8"	10"
N	4"	6"	8"	10"
O	4"	6"	8"	10"
P	4"	6"	8"	10"
Q	4"	6"	8"	10"
R	4"	6"	8"	10"
S	4"	6"	8"	10"
T	4"	6"	8"	10"
U	4"	6"	8"	10"
V	4"	6"	8"	10"
W	4"	6"	8"	10"
X	4"	6"	8"	10"
Y	4"	6"	8"	10"
Z	4"	6"	8"	10"

**DETAIL CONCRETE THRUST BLOCKS**  
NO SCALE



**DETAIL FIRE HYDRANT INSTALLATION**  
NO SCALE



**DETAIL TYPICAL TRENCH SECTION**  
NO SCALE

DRUMMEY  
ROSENE  
ANDERSON  
INC.

Colby Hall  
141 Merrick Road  
P.O. Box 299  
Newton Centre, MA  
02459-0299

Architecture  
Interior Design

617-961-1788

**WESTFORD ACADEMY**

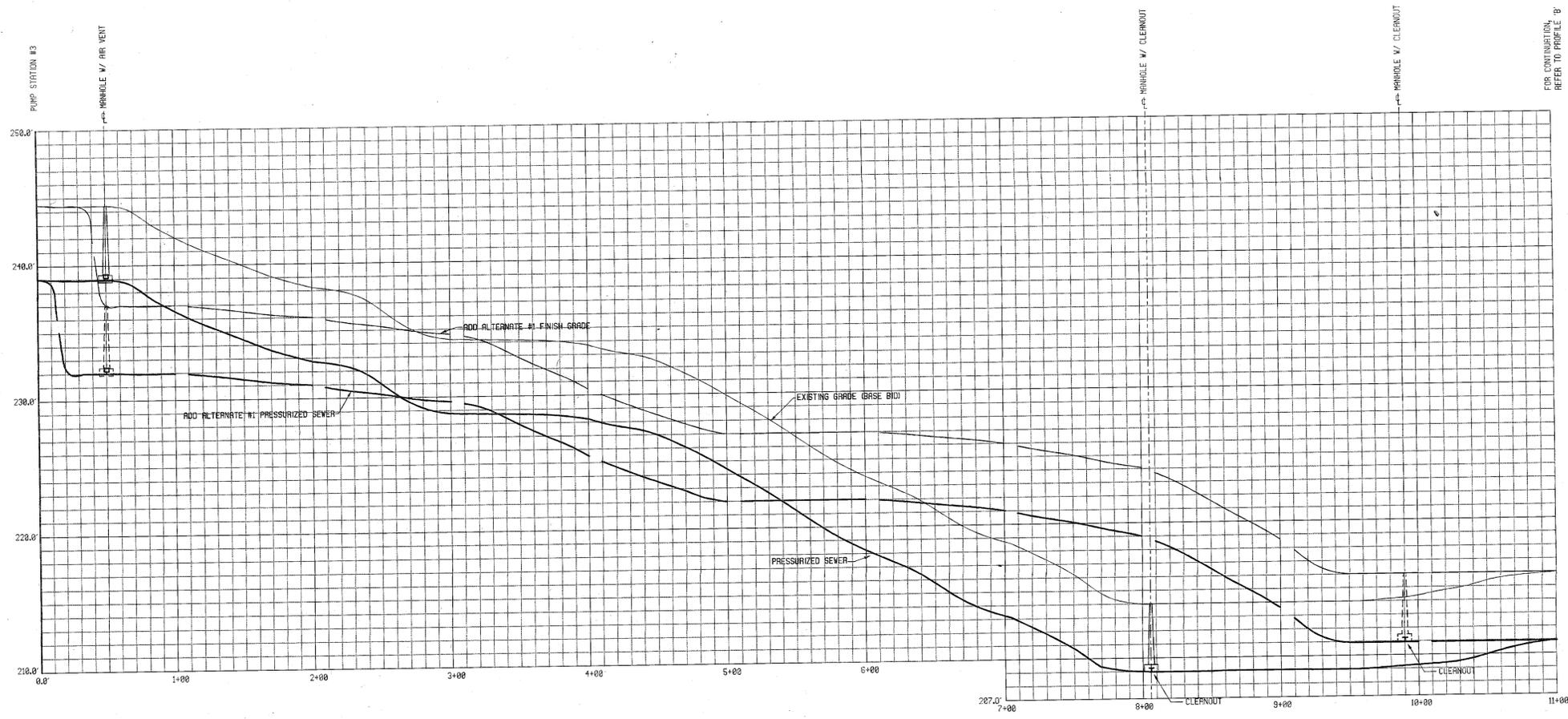
**WESTFORD MASSACHUSETTS**



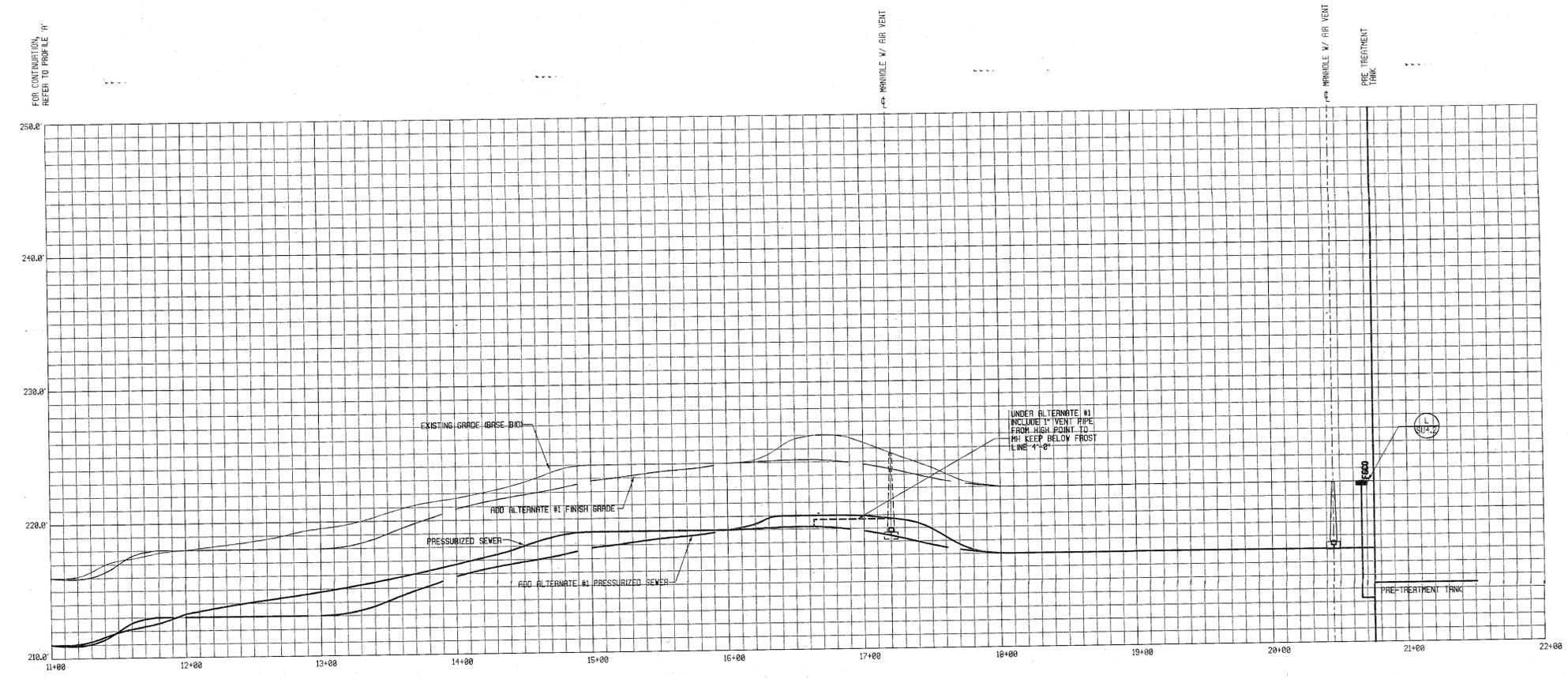
**SITE PLAN  
SITE SUITABILITY  
ASSESSMENT**

Scale: NONE  
Dr. By: CST  
Job No.: 92-183a  
Date: 01/14/98

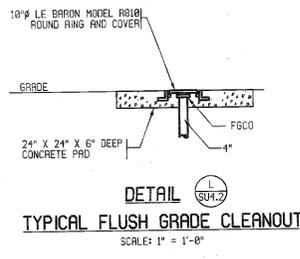
SU4.1



**PROFILE 'A'**  
 HORIZONTAL SCALE: 1"=40'-0"  
 VERTICAL SCALE: 1"=4'-0"



**PROFILE 'B'**  
 HORIZONTAL SCALE: 1"=40'-0"  
 VERTICAL SCALE: 1"=4'-0"



**D·R·A**  
 DRUMMEY, ROSSNE, ANDERSON, INC.  
 Colby Hall, 141 Herrick Road, P.O. Box 289, Newton Centre, MA, 02159-0289  
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**WESTFORD ACADEMY**

**WESTFORD MASSACHUSETTS**

*M.P. 21c Original*  
 88-41-1

D.E.P. REVISION 10-17-97  
 D.E.P. REVISION 8-28-97



**SITE UTILITY PROFILES**

Scale: AS NOTED  
 Dr. By: CST  
 Job No.: 92-103b  
 Date: 01/14/98  
**SU4.2**

92-103b